

NIVA  
Oslo

C 2-33

0-117/76

SYSTEMANALYSE AV  
SLAMHANDTERING

DELRAPPORT 2

Oslo, 1. april 1980

Saksbehandlar: Kjell Øren

Medarbeidar: Thor Adriansen

Instituttstjef: Kjell Baalsrud

# NIVA - RAPPORT

Norsk institutt for vannforskning



NIVA

Norges Teknisk-Naturvitenskapelige Forskningsråd

Postadresse: Brekke 23 52 80  
Postboks 333, Blindern Gaustadalleen 46 69 60  
Oslo 3 Kjeller 71 47 59

|                         |         |
|-------------------------|---------|
| Rapportnummer:          | 0-76117 |
| Undernummer:            | II      |
| Løpenummer:             | 1254    |
| Begrenset distribusjon: |         |

|                                 |                                       |
|---------------------------------|---------------------------------------|
| Rapportens tittel:              | Dato:                                 |
| SYSTEMANALYSE AV SLAMHANDTERING | 8/12 1980                             |
| Delrapport 2                    | Prosjektnummer:                       |
|                                 | 0- 76117<br>C2 - 33                   |
| Forfatter(e):                   | Faggruppe: SEKVAT<br>SEKSPS<br>ANADAT |
| Siv.ing Thor Adriansen          | Geografisk område:                    |
| Siv.ing Kjell Øren              | Antall sider (inkl. bilag):           |
|                                 | 150                                   |

|  |                                  |
|--|----------------------------------|
| Oppdragsgiver:   | Oppdragsg. ref. (evt. NTNf-nr.): |
| NTNF's utvalg for fast avfall<br>Norsk institutt for vannforskning | 1.2.17                           |

Ekstrakt:

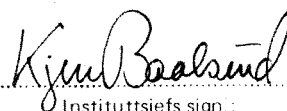
Rapporten er delt i to: DEL A gjev eit grovt oversyn over slamproblemet i Noreg. Ved århundreskiftet vil det bli produsert omlag 130 000 tonn TS/år som kommunalt slam, av dette omlag 75 % frå reinseanlegg med kjemisk felling. 2/3 av slammet kjem frå anlegg med meir enn 5000 pe tilknytt. Eit forsøk på systematisering av slamhandtering og prosesskombinasjonar er gjort. DEL B skildrar l. utgåva av modellprogrammet PREDES, som reknar massebalansar i reinseanlegg ut frå brukarspesifiserte føresetnader.

|                         |
|-------------------------|
| 4 emneord, norske:      |
| 1. systemanalyse        |
| 2. slambehandling       |
| 3. avløpsvarnbehandling |
| 4. matematisk modell    |

|                         |
|-------------------------|
| 4 emneord, engelske:    |
| 1. system analysis      |
| 2. sludge handling      |
| 3. wastewater treatment |
| 4. mathematical model   |

  
Prosjektleders sign.:

  
Seksjonsleders sign.:

  
Institutt sjefs sign.:

ISBN 82-577-0336-2

## FØREORD

På oppdrag frå NTNf's utval for fast avfall har NIVA arbeidd med prosjektet "Systemanalyse av slamhandtering". NIVA har samstundes ytt forskningsmidlar til prosjektet "Systemanalyse av reinseprosesser". Føreliggjande rapport omfattar begge desse prosjekta.

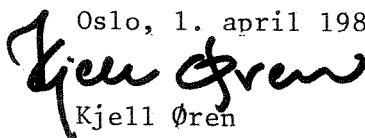
Av praktiske grunnar er rapporten delt i to. Del A gjer bakgrunnsinformasjon og oversyn over problema frå norsk synsstad, medan del B skildrar sjølve modellpakken som er utvikla. Av omsyn til seinare bruk og spreing av modellen, er det vurdert føremålstenleg å skriva del B på engelsk.

Sivilingeniør Thor Adriansen har hatt ansvaret for det datatekniske opplegget, og har saman med underskrivne utforma denne rapporten.

Professor Peter Balmér ytte stor hjelp i ein tidleg fase av prosjektet, og har også vore med på utarbeiding av ein del av prosessmodellane.

Balmér har også gjennomgått og kommentert denne rapporten. Tusen takk for all inspirasjon, Peter!

Oslo, 1. april 1980

  
Kjell Øren

|  |      |
|--|------|
| INNHALD  | Side |
| FØREORD  | 3    |
| DEL A  |      |
| 1. INNLEIING                                   | 5    |
| 1.1 Bakgrunn og status                         | 5    |
| 1.2 Avgrensingar                               | 7    |
| 2. FÅR VI ET SLAMPROBLEM I NOREG?              | 8    |
| 2.1 Slamproduksjon år 2000                     | 8    |
| 2.2 Disponering på dyrka mark krev store areal | 11   |
| 2.3 Arealbehovet ved deponering                | 12   |
| 3. FORSØK PÅ SYSTEMATISERING                   | 14   |
| 3.1 Faktorar som påverkar slambehandlinga      | 14   |
| 3.2 Krav til slamproduktet                     | 17   |
| 3.3 Karakterisering av slamproduktet           | 21   |
| 3.4 Endring av karakteristika i prosessane     | 23   |
| 4. PLANLEGGING PÅ ULIKE NIVÅ                   | 24   |
| 4.1 Typiske planleggingsfasar                  | 24   |
| 4.2 Materialbalanse-opplegg                    | 24   |
| 5. REFERANSAR                                  | 25   |
| DEL B  |      |
| Brukarinstruks for EDB-programmet PREDES       | 26   |

## 1. INNLEIING

### 1.1 Bakgrunn og status

Innan PRA-prosjekta var det tidlegare utvikla enkle modellar både for reinseanlegg og slambehandling. Prosjektet "Systemanalyse av slamhandtering" tok utgangspunkt i desse modellane. Sjølv om ein vurderte dei aktuelle kombinasjonane av slamhandtering til å vera relativt avgrensa, fann ein det tenleg å utvikla modellane. I eit tidlegare prosjektnotat frå NIVA er dette vurdert såleis:

- " - Det vil gi muligheter for meget lett å beregne slamproduksjon og materialstrømmer for aktuelle anlegg. Dette burde kunne spare mye beregningsarbeide for rådgivende ingeniører.
- Skal en kunne analysere samspillet mellom ulike slambehandlingsenheter, vil modeller trolig være et nødvendig verktøy. Det bør imidlertid bemerkes at kunnskapene om en del slambehandlingsoperasjoner og slamkvaliteter i dag ikke er tilstrekkelig for en slik analyse."

Med utgangspunkt i dei enkle modellane som tidlegare var utvikla ved NIVA, vart difor følgjande arbeidsopplegg føreslege:

### ARBEIDSOPPLEGG

- "1. Kritisk gjennomgåelse av eksisterende modell for slamproduksjon. Nødvendige forbedringer gjøres, og modeller testkjøres mot reelle data.
2. Forbedringer av eksisterende modell for slambehandling.
  - a) Det sett av ligninger som er innlagt i modellen, gjennomgås kritisk, og de nødvendige forandringer gjennomføres. Modellen testes og forandres inntil resultatene skjønsmessig bedømmes som fornuftige.
  - b) Flere sekvenser av slambehandlingsoperasjoner enn de syv som nå finnes i modellen, innføres. De nødvendige testkjøringer gjennomføres.

- c) Ved slambehandling (f.eks. stabilisering) kan slammet undergå kvalitetsforandringer (f.eks. avvannbarhet) som er av liten betydning ved den endelige disponering, men som kan være svært vesentlige ved valg av slambehandling og for dimensjonering av de enkelte slambehandlingsoperasjoner. Det bør vurderes i hvilken utstrekning det er mulig å innføre funksjoner i modellen som gjør det mulig å ta hensyn til slike forhold.
- 3. Modellen utvikles slik at det er mulig å få med andre parametre enn tørrstoff.
- 4. Ytterligere videreutvikling av modellen f.eks. at
  - a) rekkefølgen av slambehandlingsoperasjoner generaliseres slik at en ikke er bundet til gitte sekvenser.
  - b) modellene for de enkelte slambehandlingsoperasjoner detaljeres slik at det blir mulig å analysere samspillet mellom ulike slam- og vannbehandlingsoperasjoner og å optimalisere dette system. Det er mulig at en videreutvikling av denne type vil gjøre det nødvendig å gå over til en dynamisk modell."

Status for dei einskilde punkter er:

- 1. Utført. Resultat og føresetnader er gitt i delrapport 1 (1).
- 2a) Likningane er gjennomgått. Ut frå dette er det vurdert nødvendig å prøva detaljera prosessmodellane i større grad, og bygga opp ein ny modell. Punkt 2a) er difor ikkje fullt ut gjennomført.
- b) Utført. Det er nytta ei fleksibel modelloppbygging.
- c) Arbeidet er komplisert, og det har ikkje vore mogeleg å få inn dei funksjonane det er nemnt.
- 3. Utført.
- 4a) Utført - bruk av fleksibel oppbygging.
- b) Ingen optimalisering er utført.

## 1.2 Avgrensingar

Modellsystemet som er presentert i denne rapporten, har ein del avgrensingar, som fell i to hovudgrupper:

### a) Prosesstekniske

dvs. i utvalet av prosessar og sjølve prosessmodellane. Det har vore gjort ein heil del praktiske forsøk med ulike prosessar. Totalt sett er det likevel gjort relativt lite forsøk på å generalisera resultatata.

Dei prosessmodellane som er nytta, er så langt råd er bygt kring eit teoretisk fundament. I fleire tilfelle er det likevel gjort "kortsluttingar", fordi grunnlag og tid for ei meir detaljert skildring ikkje har vore tilstades.

Omfattande testing av modellane mot praktiske målingar har det ikkje vore høve til å gjennomføra.

### b) Systemoptimalisering

Modellsystemet krev at brukaren spesifiserar flytskjemaet for det aktuelle reinseanlegget, og det er førebels ikkje lagt inn optimaliseringsrutiner for denne gitte kombinasjonen.

Det eksisterer heller ikkje rutiner for kombinasjon av prosessar ut frå gitte sluttkrav.

Økonomiske parametrar er heller ikkje med i denne omgang, men er lett å leggja inn i tilknytting til dei einskilde prosessane.

Trass i desse avgrensingane, vil programmet vera til hjelp for både planlegging, dimensjonering og driftsanalyse av reinseanlegg. På enkel måte får ein rekna massebalansar, og får verdiar for eit stort tal parametrar.

## 2. FÅR VI EIT SLAMPROBLEM I NOREG?

Interessa for behandling og disponering av slam frå kommunale reinseanlegg er aukande. For å setja ei grov råde kring omfang og storleiksorden, er det nedanfor gjort eit enkelt overslag.

2.1 Kommunalt slam i storleiken 130.000 tonn TS/år vil produserast ved århundreskiftet. 2/3 av dette slammjet kjem frå reinseanlegg med meir enn 5000 p.e. tilknytta.

Når planlagde tiltak i norske byar og tettstader er gjennomførde, vil ein ved århundreskiftet produsera kloakkslam i storleiksorden 130.000 TS/år. Omlag 75 prosent av dette vil vera slam frå reinseanlegg med kjemisk felling i ei eller anna form.

Ut frå grunnlagsmaterialet til St.meld. 107 (1974-75) "Om arbeidet med en landsplan for bruken av vannressursene" (2) er kommunale reinseanlegg fordelt etter storleik år 2000 og synt i figur 1. Figur 2 syner grovt dei slammengdene som vi i gjennomsnitt kan rekna for kvart anlegg i dei ulike storleiksgruppene, og i figur 3 er dei totale slammengdene fordelt etter storleiken på reinseanlegga.

Vi kan gjera ein del interessante refleksjonar ut frå figurane. M.a. ser vi at reinseanlegg i gruppa over 5000 p.e. utgjer berre 13 prosent av det totale tal reinseanlegg, men står likevel for 65 prosent av dei slammengdene som blir produsert.

I så måte finn ein litt av grunnen til at slammjet ofte blir sett på som eit problem. I større byar og tettstader der slammengdene blir store, er det også vanskelegast å finna eigna disponeringsform og -stad for produktet.

Det er store ønskje om å bruka slammjet på jord- og skogareal, parkar og grøntanlegg, på vegfyllingar. Bruken av slammjet er i dag underlagt restriksjonar frå helse- og veterinærstyresmakter, jordbruksinteresser og forureiningstilsyn. I kor stor grad slammjet kan brukast vidare, er difor ikkje åleine bestemt av transportøkonomiske vurderingar, men av kvaliteten på slamproduktet ein får fram.



Fig.1. Renseanlegg fordelt på størrelse i år 2000.

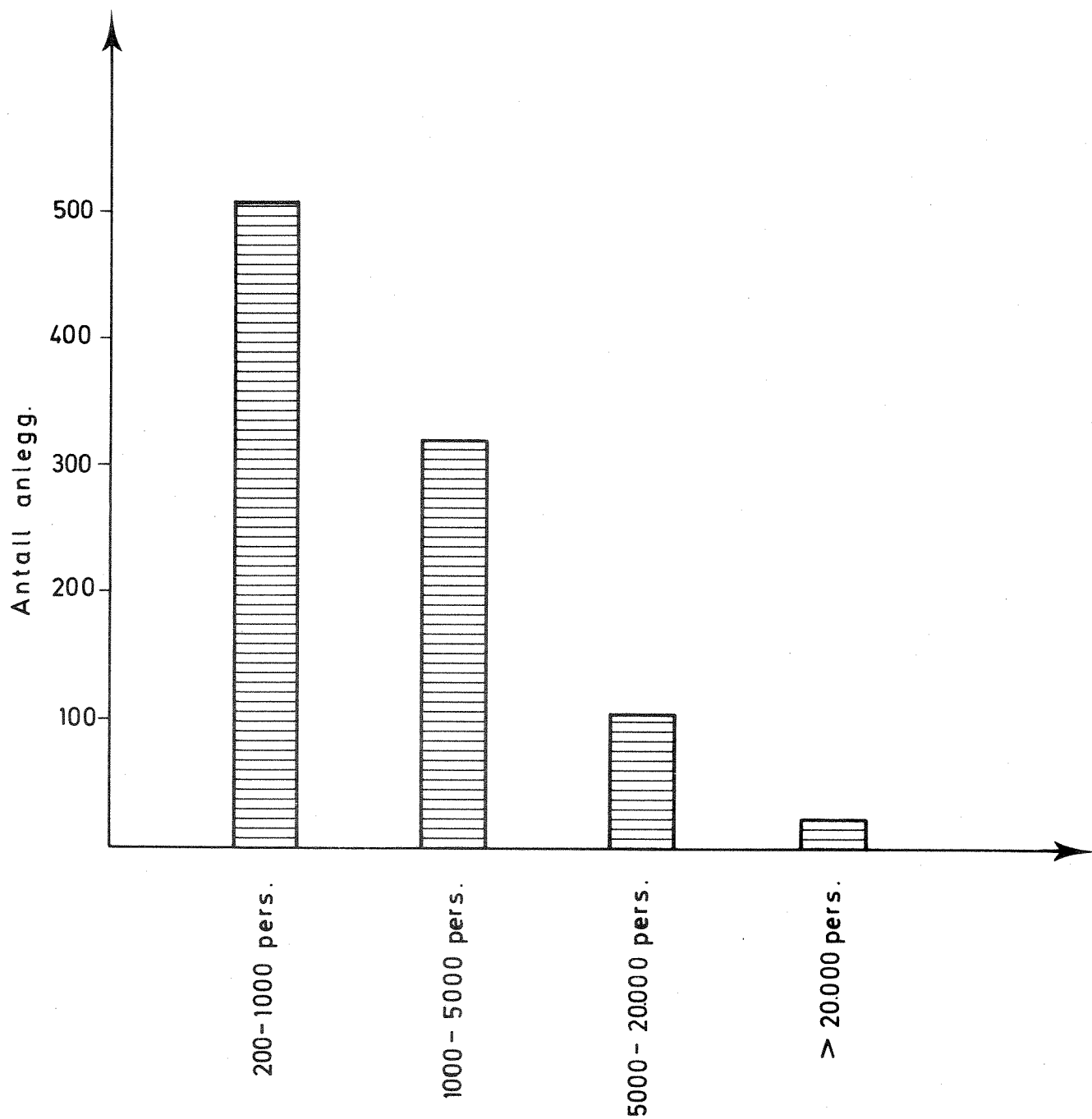
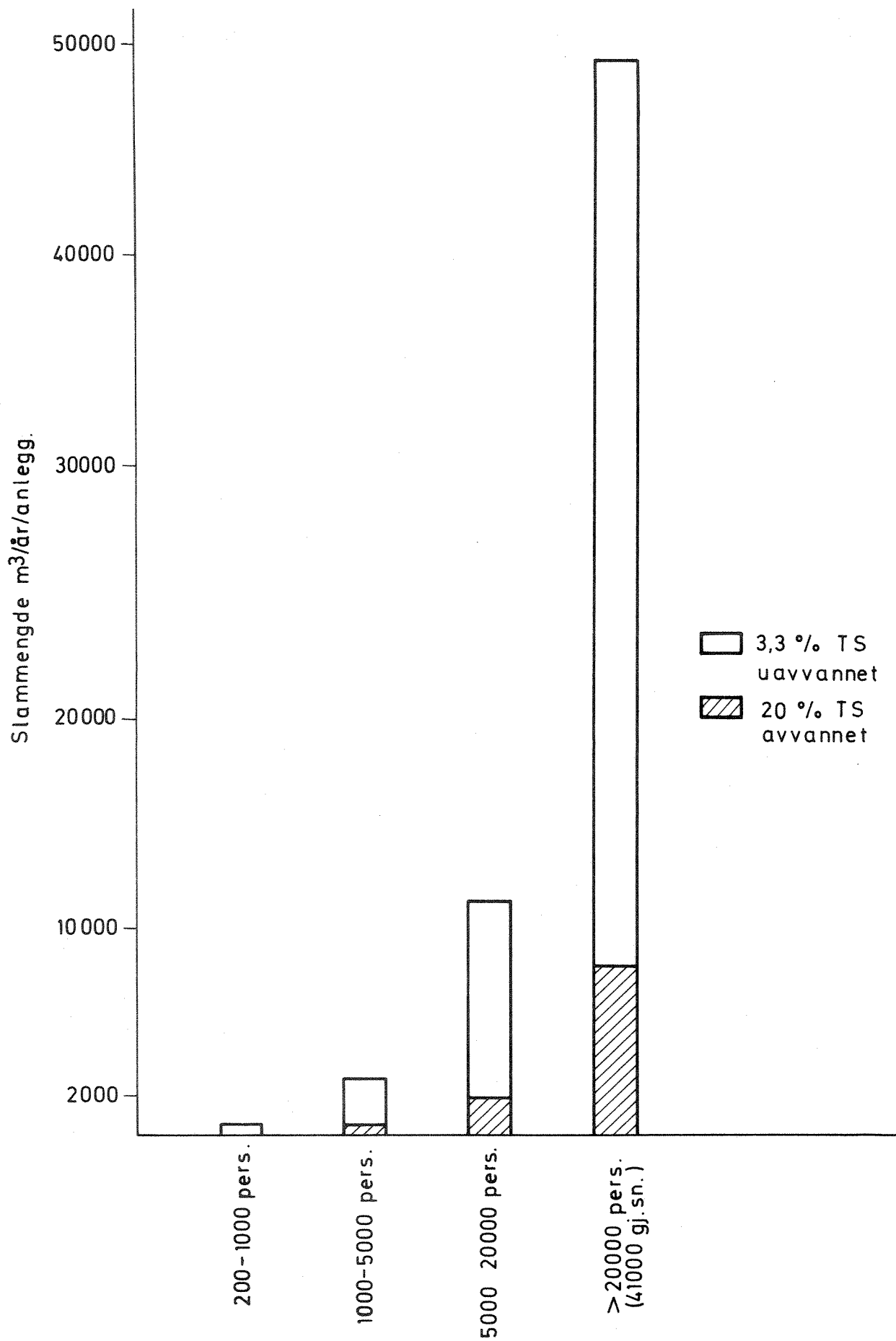


Fig. 2. GJENNOMSNI TTLE G SLAMPRODUKSJON PR. ANLEGG I DEI ULIKE STORLEIKSGRUPPENE



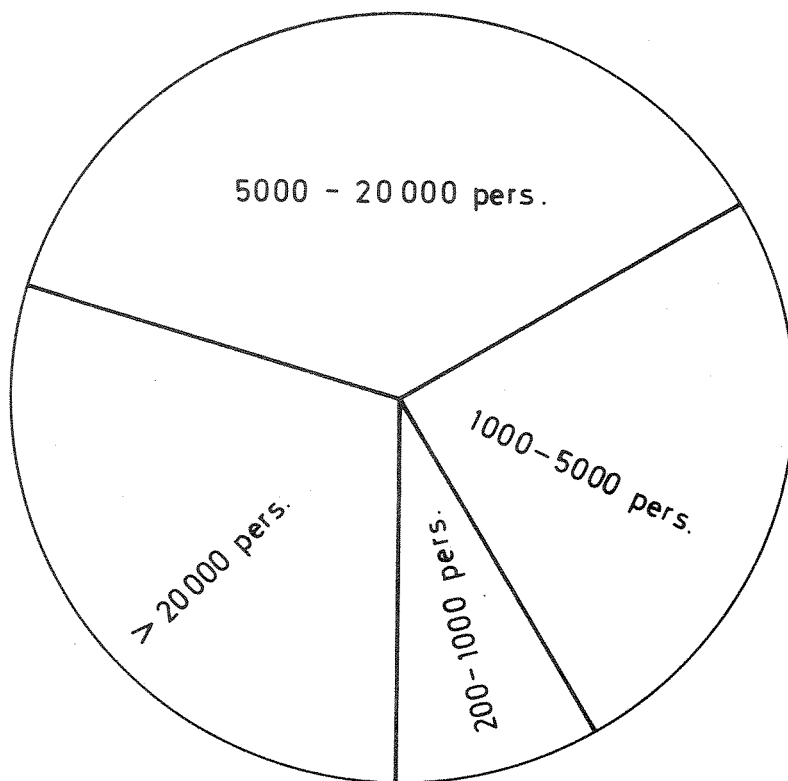


Fig. 3. Total slammengde, fordeling på renseanleggets størrelse.

Ønskjer ein derimot å leggja slammet bort - deponering, er dette først og fremst regulert gjennom helse- og forureiningstilsyn.

For å gje eit lite oversyn over to ytterpunkt for slamdisponering, bruk på dyrka mark og rein deponering i fylling, har vi sett på arealbehovet ved desse to bruksmåtane.

## 2.2 Disponering av slammet på jordbruksareal etter Helsedirektoratet si rettleiing krev store areal.

Helsedirektoratet har gjeve ut ei rettleiing til helseråda om m.a. bruk av slam på jordbruksareal (3).

Vi føreset at slammet har gått gjennom behandling som støttar Helsedirektoratet sine brukskrav. Dersom alt slammet frå reinseanlegg i ein del utvalde

fylke år 2000 skal disponerast på jordbruksareal etter Helsedirektoratet si rettleiing (1 tonn TS/da/5 år), får vi følgjande arealbehov:

Tabell 1. Arealbehov ved slamdisponering på dyrka mark.

| Fylke           | Arealbehov | % av fylket sitt totale areal | % av fylket sitt landbruksareal |
|-----------------|------------|-------------------------------|---------------------------------|
| Oslo/Akershus   |            | 3,6                           | 23                              |
| Hedmark         |            | 0,15                          | 4                               |
| Møre og Romsdal |            | 0,3                           | 8                               |
| Finmark         |            | 0,03                          | 20                              |

Slik rettleiinga er forma i dag, fører den til at eit slam med 20% TS må leggjast ut i eit lag som er 1 mm tjukt, og det er sjølvstg dette som er årsaka til dei store arealbehova.

### 2.3 Arealbehovet ved disponering på dyrka mark er jamført med deponering av 50 års akkumulert slamproduksjon

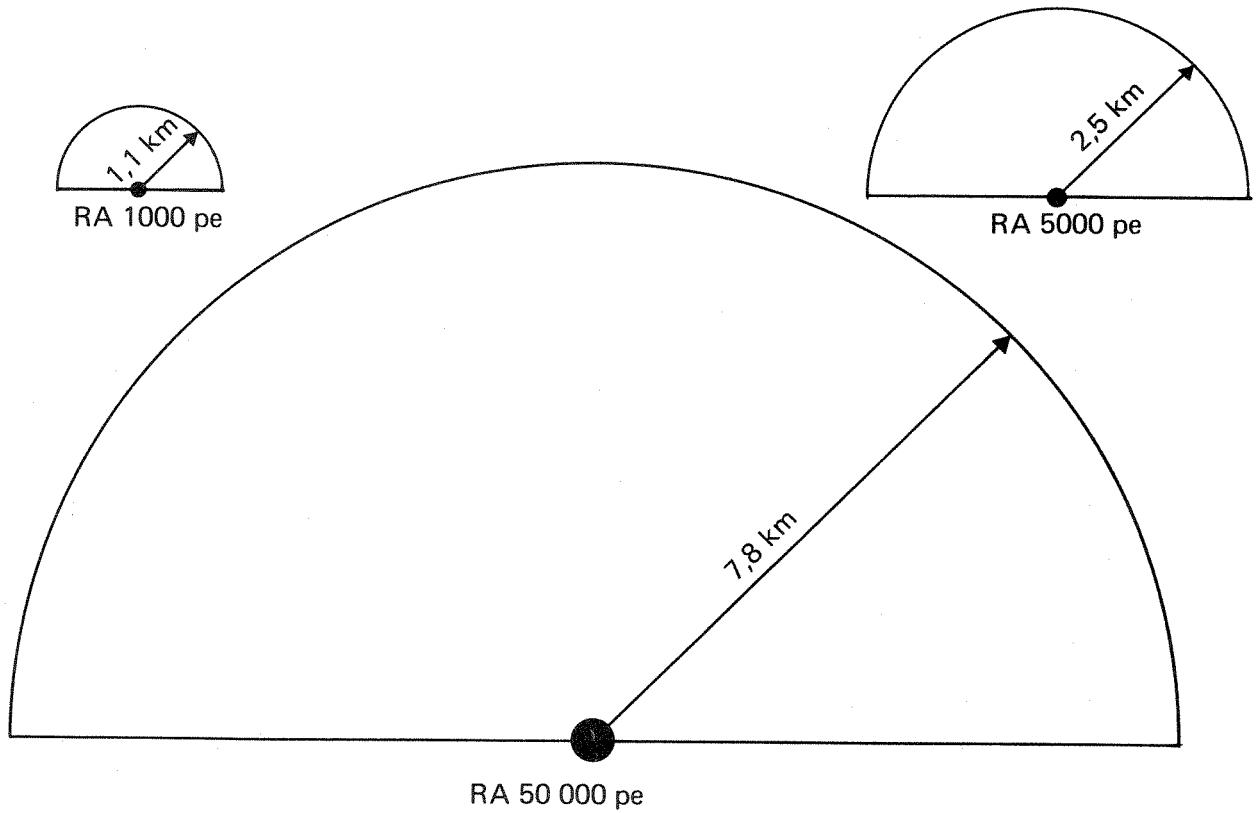
For reinseanlegg med 1000, 5000 og 50.000 p.e. tilknytta syner figur 4 arealbehovet ved disponering på jordbruksareal og rein deponering. Ved disponering har vi pårekna at 10 prosent av arealet kring reinseanlegget kan nyttast.

Ved deponering har vi pårekna avvatna slam med 20 prosent TS, og figur 5 syner kva areal som er nødvendig for å samla opp 50 års akkumulert slamproduksjon for ulike anleggsstorleikar, dersom vi legg slammet i 3 m høgd.

Figurane 4 og 5 kan vera nyttige for å setja det vi nemner "slamproblem" i rett perspektiv.

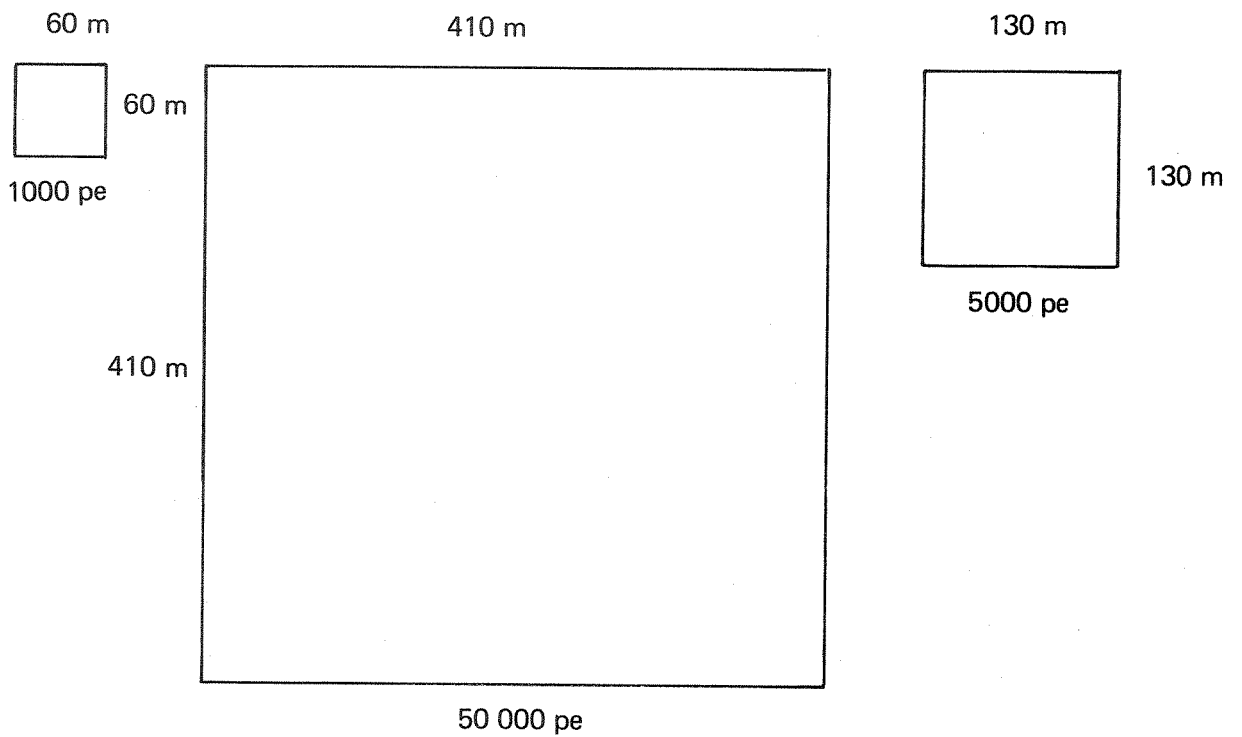
AREALBEHOV VED SPREIING PÅ DYRKA MARK.  
10% AV AREALET KAN NYTTAST, TJUKN SLAMLAG 1MM

Fig. 4



AREALBEHOV VED DEPONERING AV SLAM - 20% TS -  
50 ÅRS AKKUMULERT SLAMPRODUKSJON I 3 M HØGD

Fig. 5



### 3. FORSØK PÅ SYSTEMATISERING

#### 3.1 Faktorar som påverkar slambehandlinga

Figur 6 syner det viktige samspelet mellom vass- og slambehandlinga i eit reinseanlegg.

Tradisjonelt er det sett krav til det reinsa avløpsvatnet ut frå resipientvurderingar. Meir sjeldan er det slamproduktet som kjem fram ofra omtanke, og ordet "problem" er ofte nemnt.

Det ideelle er at ein set krav både til det reinsa avløpsvatnet og til det slamproduktet ein får fram, slik fig. 7 framstiller.

Vurdert med tanke på slamsida, kan figuren forklarast slik:

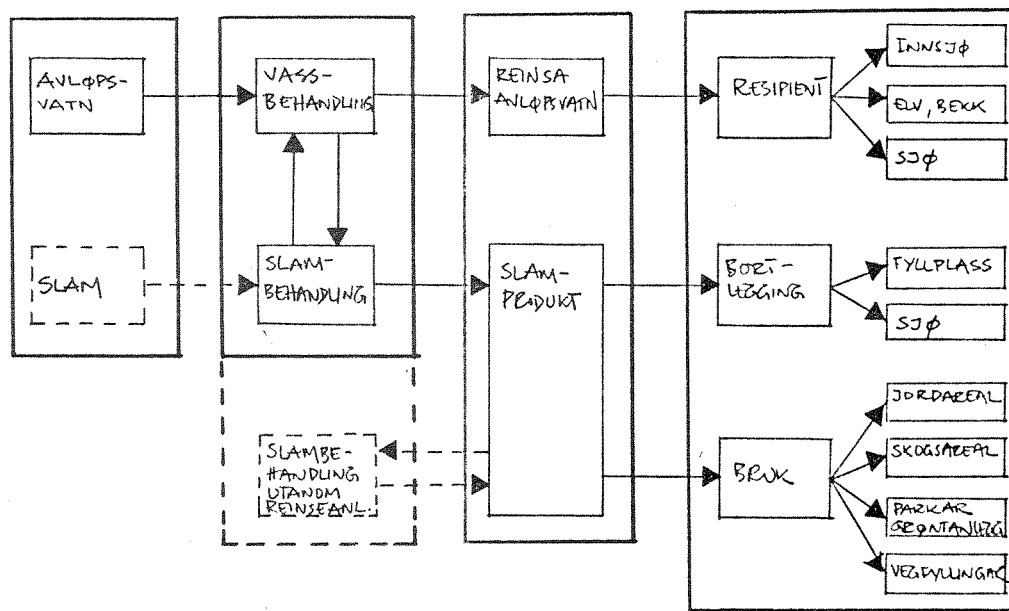


FIG. 6. SKISSE OVER SAMPELET VASS- OG SLAMHANDTERING

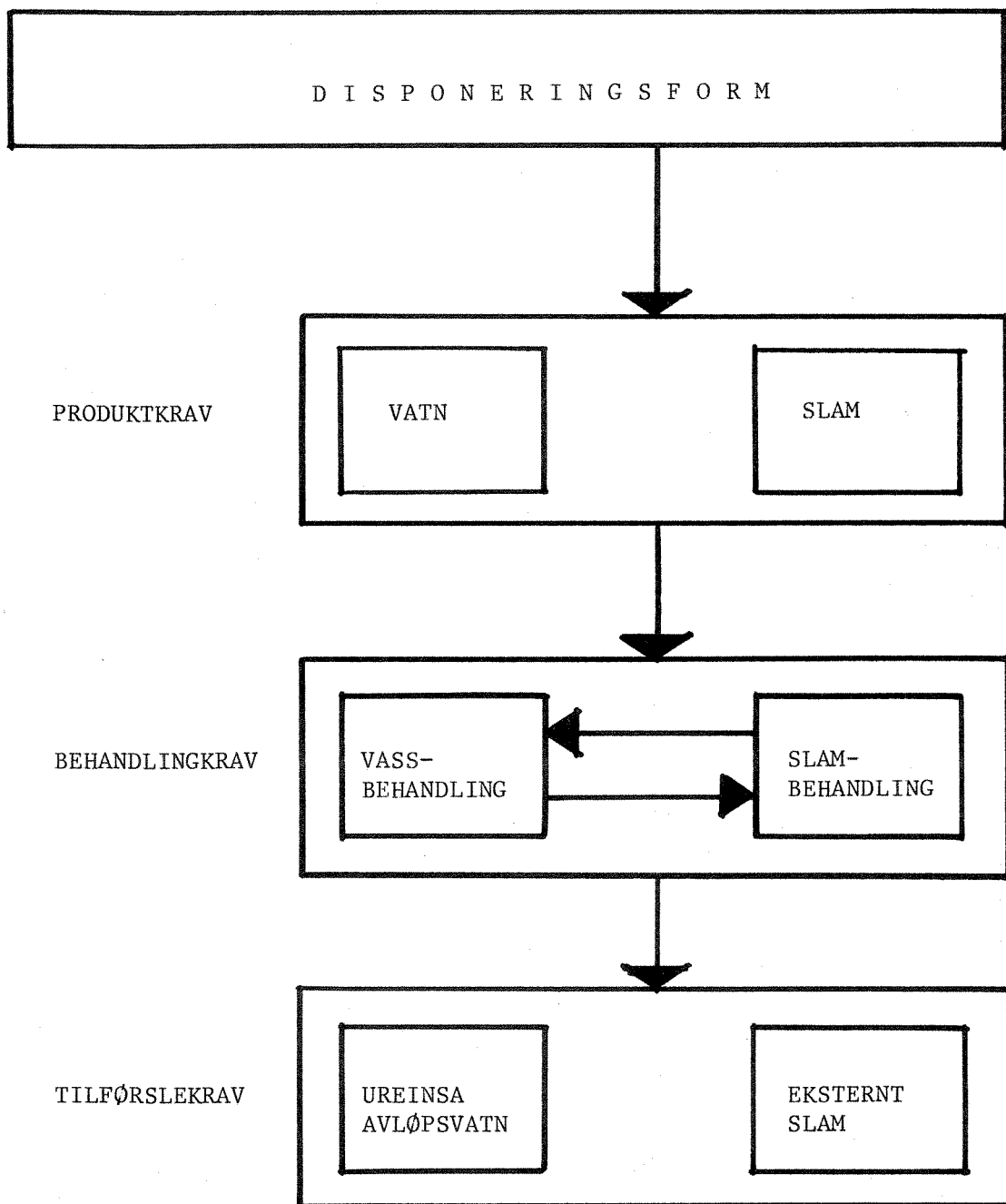


FIG. 7. SAMANHENG MELLOM SLAMDISPONERING OG SLAMBEHANDLING

Slammet frå kloakkreinseanlegg går til

- a) bruk (i vid forstand)
- b) bortlegging

Disponeringa av slamproduktet set såleis ulike krav til slameigenskapane. I prinsippet kan desse krava oppfyllest ved å stilla krav til slambehandlinga. Einskilde krav (m.a. tungmetallinnhald) kan likevel berre oppfyllest ved bruk av avanserte prosessar som er lite aktuelle for norske tilhøve. I staden er det difor naturleg å setja krav til kvaliteten av eksterne tilførsler.

Frå disponeringssynspunkt vil ein få fram eit sett av alternative slambehandlingsprosessar som kan oppfylla krava til slamproduktet. Andre tilhøve kan likevel krevja eliminering av nokre prosessar eller at andre prosessar vert sett inn i tillegg.

T.d. er det nært samband mellom slam- og vassbehandlinga i eit reinseanlegg. Slambehandlingsprosessane vil oftast gje eit slamvatn som vert ført tilbake til vassbehandlingsdelen, og i sin tur kan forstyrre vassprosessane. Som døme kan nemnast tilførsler av slamvatn frå eksternt septikslam, og slamvatn frå kalkstabilisering i kjemiske fellingsanlegg med aluminiumsulfat. Krava til vassbehandling stiller såleis eigne krav til slambehandlinga.

Av dette går det fram at slamdisponeringa aleine ikkje er avgjerande for val av slambehandlingsprosessar.

Etter vurderingane framanfor vil valet av slamhandtering koma fram som følgje av:

- 1) Krav til slameigenskapar, gitt av disponeringa. (Føresetnaden er at slameigenskapane kan endrast gjennom behandlingsprosessar).
- 2) Krav til vassbehandlinga, dvs. val av prosessar og omsynet til drift av desse.
- 3) Krav til tilførsler av tungmetall og andre miljøgifter (via eksternt slam- og avløpsvatn).



### 3.2 Krav til slamproduktet

Dei krava ein stiller, er ein funksjon av behov, tilgjengeleg teknologi og økonomiske utteljingar.

Om vi i det følgjande vurderer kun slamsida, kan vi oppsummera:

#### Behov

Krava byggjer på at ein skal gjera minst mogeleg skade på omgivnadene og er førebels regulert gjennom lover, føreskrifter, retningslinjer m.v. Av dei viktigaste kan nemnast:

Tabell 2. Oversyn over lover, retningslinjer m.v. som regulerer slamdisponeringa.

| Regulert gjennom:        | Gjeldande lover, føreskrifter m.v.  |
|--------------------------|---|
| Helsestyresmakter        | <ul style="list-style-type: none"><li>o Sunnhetsloven (1860)</li><li>- forskrifter om oppbevaring av avfall og om renovasjon (1970)</li><li>- forskrifter om hygieniske forhold i hytteområder o.l. (1970)</li><li>- hygienisk vurdering av kloakkslam - en veiledning for helserådene (1976)</li></ul> |
| Arbeidsmiljøstyresmakter | <ul style="list-style-type: none"><li>o Arbeidsmiljøloven m/føreskrifter</li></ul>  |
| Landbruksstyresmakter    | <ul style="list-style-type: none"><li>o Plantesjukdomslova</li></ul>  |
| Veterinærstyresmakter    | <ul style="list-style-type: none"><li>o Husdyrlova</li></ul>  |
| Miljøvernstyresmakter    | <ul style="list-style-type: none"><li>o Lov om vern mot vannforurensning (1970)</li><li>- retningslinjer for deponering av kommunalt avfall i fylling (1978)</li><li>- bygningslova (1965)</li></ul>  |

Av gjeldande reglar er det Helsedirektoratet si rettleiing ("Hygienisk vurdering av kloakkslam" (3)) som mest direkte regulerer bruken av slam. Statens forureiningstilsyn (SFT) har no under utarbeiding nye retningslinjer for slamdisponering, og ein vil difor ikkje gå nærare inn på dette her.

#### Tilgjengeleg teknologi

Mange prosessar er aktuelle for slambehandlinga. Tabell 3 syner dei prosessane og prosesskombinasjonane som kan reknast bli vurdert i Noreg. Prosesskombinasjonane er gjort ut frå ei skjønsmessig vurdering. Openberre umogelege kombinasjoner er utelatne (som t.d. forbrenning før fortjukking.)

#### Økonomi

Legg vi skjønsmessige økonomiske vurderingar til grunn, attåt ei vurdering av eksisterande praksis, vil vi truleg enda opp med ei prosessmatrise som i tabell 4. Denne matrisa inneheld ei vurdering av prosessane i tabell 3, og utgjer det utvalet av slambehandlingsprosessar som vi i dag vurderer som mest aktuelle for våre norske, heller små anlegg. Forbehandlingsprosessar er sjølvsagt aktuelle, men er ikkje med i matrisa.





### 3.3 Karakterisering av slamproduktet

I punkt 3.2 er krav til slamproduktet nytta som stikkord. Skal desse krava vera til hjelp i planlegging og dimensjonering av slambehandlingsanlegg, må dei både klassifiserast og kvantifiserast.

Sett frå kun disponeringssynsstad, kan hovudklassifikasjonen vera som i tabell 5.

Tabell 5. Hovudklassifikasjon av disponeringskrav.

| HOVUDASPEKT                 | UTTRYKT VED PARAMETER           | VURDERING AV MÅLESKALA |       |           |
|-----------------------------|---------------------------------|------------------------|-------|-----------|
|                             |                                 | OBJEKTIV               | UKLAR | SUBJEKTIV |
| HANDTERING                  | VOLUM                           | X                      |       |           |
|                             | TØRRSTOFF                       | X                      |       |           |
|                             | STRUKTUR                        | (X)                    |       | X         |
| HYGIENE<br>HELSEVERN        | VIRUS, BAKTERIAR,<br>PARASITTAR |                        | X     | X         |
|                             | TUNGMETALL                      | X                      |       |           |
| PÅVERKNAD AV<br>OMGJEVNADER | LUKT - TYPE                     |                        |       | X         |
|                             | - INTENSITET                    | (X)                    |       | X         |
|                             | AVRENNING - MENGDE              | X                      |       |           |
|                             | - KVALITET                      | X                      |       |           |
| ANDRE BRUKSKRAV             | ORGANISK MATERIALE              | X                      |       |           |
|                             | NÆRINGSEMNE                     | X                      |       |           |
|                             | PLANTEVERN                      |                        | X     | X         |

Tabell 5 byggjer på subjektive vurderingar. Tabellen syner likevel ein del av spennvidda når det gjeld slamkarakterisering. For handteringsparameteren struktur kan vi operera med omgrep som spabar, pulveraktig m.v., men sjølve parameteren er vanskeleg å talfesta objektiv.

Helseparametrane virus, bakteriar og parasittar er også dels tvilsame. Måleteknisk er det vanskeleg å få fram reproduerbare verdiar, og det vil mest alltid bli nødvendig med ei grov subjektiv vurdering av desse tilhøva. Luktparametrane er viktige, men er i tabellen klassifisert som subjektive på måleskalaen. Det same gjeld delvis plantevern. Sjølv om parametrar ikkje kan kvantifiserast direkte, er dei like viktige for det. Ei rein subjektiv, relativ vurdering er sjølv sagt ikkje så akademisk tilfredsstillande, men er fullt mogeleg.

Tabell 6 syner eit parametersett som er nytta i modellen presentert i del B av denne rapporten. Parametrane er valde ut frå det totalsystemet som er forsøkt skildra, og ein del parametrar som er turvande for vassfasen er med.

Tabell 6. Parametersett for skildring av slamkvalitet.

| PARAMETER                 | EINING              | PARTIKULERT MATERIALE | LØYST MATERIALE |
|---------------------------|---------------------|-----------------------|-----------------|
| Suspendert stoff          | kg/m <sup>3</sup>   | x                     |                 |
| Flyktig suspendert stoff  | kg/m <sup>3</sup>   | x                     |                 |
| Biokjemisk oksygenforbruk | kg/m <sup>3</sup>   | x                     | x               |
| Fosfor                    | kg/m <sup>3</sup>   | x                     | x               |
| Nitrogen                  | kg/m <sup>3</sup>   | x                     | x               |
| Kadmium                   | g/m <sup>3</sup>    | x                     | x               |
| Kvikksølv                 | g/m <sup>3</sup>    | x                     | x               |
| Bly                       | g/m <sup>3</sup>    | x                     | x               |
| Kalsium                   | kg/m <sup>3</sup>   | x                     | x               |
| Magnesium                 | kg/m <sup>3</sup>   | x                     | x               |
| Alkalitet                 | ekv./m <sup>3</sup> |                       | x               |
| pH                        |                     |                       | x               |
| Hygiene                   | -                   | x                     |                 |
| Lukt                      | -                   | x                     |                 |
| Plantevern                | -                   | x                     |                 |

Ein merkar seg at parametrane hygiene, lukt og plantevern er føreslått gitt talverdiar etter ein subjektiv skala.

#### 3.4 Endringar av karakteristika i prosessane

Alle slambehandlingsprosessar har til føremål å endra ein eller fleire karakteristika ved slammet. I kor stor mon desse endringane er avhengig av det slammet som kjem inn til prosessen, varierer frå prosess til prosess. Det er førebels sett mest tenleg å bruka kun parametrar som har praktisk verdi, og det tyder difor at t.d. kondisjonering og avvatningsprosessar har fått ei relativt enkel behandling vidare i denne rapporten (del B).

#### 4. PLANLEGGING PÅ ULIKE NIVÅ

##### 4.1 Typiske planleggingsfasar

Planleggings- og dimensjoneringsoppgåver for reinseanlegg m/slambehandling kan delast inn slik tabell 7 syner:

Tabell 7 Planleggingsnivå

| Nivå | Føremål                                       | Døme på aktuelle "verktøy"                                      |
|------|---|---|
| 1    | Jamføring av hovudalternativ                  | Enkle materialbalanse-modellar<br>Enkle optimaliseringsmodellar |
| 2    | Førebels dimensjonering<br>Prosessvurdering   | Enkle optimaliserings- og simuleringsmodellar                   |
| 3    | Vurdere drifts-rutiner, drifts-optimalisering | Detaljerte, dynamiske prosessmodellar                           |

##### 4.2 Materialbalanseopplegg

Eit kjernepunkt i alt som har med slam å gjera, er sjølvstapt produksjons leddet. Det er ved og i reinseanlegget ein har dei beste tilhøva for å påverka produktkvaliteten.

Difor er det absolutt turvande å vita: Kor mykje slam blir produsert ved ulike prosessar, og korleis er samspelet mellom vass- og slambehandling? Bruker vi slambehandlingsprosessar som påverkar vassfasen negativt?

Dette er bakgrunnen for at arbeidet har vore konsentrert om reinseanlegget, og at materialbalanser der står så sentralt.



5. REFERANSAR

1. Øren, Kjell et. al: Systemanalyse av slamhandtering.  
Delrapport 1: Slamproduksjon  
UFA-prosjekt 1.2.17, NIVA (1977)
2. Balmér, Peter et.al: Landsplan for bruken av vannressursene.  
Arbeidsrapport nr. 1: Kostnader for tiltak  
i byer og tettsteder, spredt i boligbebyggelse,  
fritidsbebyggelse m.v. O-150/73 NIVA (1975)
3. Helsedirektoratet, hygienekontoret:  
Hygienisk vurdering av kloakkslam.  
En veiledning til helserådene (1976).
4. Lygren, Eivind et. al: Disponering av avvannet slam.  
Sigevannsproblemer ved lagring av ulike  
slamtyper.  
UFA-prosjekt 4.3.18, O-103/77 NIVA (1978)

PART B

USER'S GUIDE FOR THE COMPUTER MODEL PROGRAM  
PREDES

## LIST OF CONTENTS

|  | Page       |
|--|------------|
| 1. OBJECTIVES FOR PROGRAM DEVELOPMENT                                      | 1.1        |
| 2. SPECIAL CHARACTERISTICS   | 2.1 - 2.3  |
| 2.1 Flow chart   | 2.1        |
| 2.2 Design flow rates  | 2.1        |
| 2.3 Stream characteristics   | 2.2        |
| 3. PROCESS DESCRIPTIONS  | 3.1 - 3.49 |
| CENTRI - Sludge dewatering   | 3.2        |
| CHEMAL - Chemical precipitation by alum                                    | 3.6        |
| CHEMCA - Chemical precipitation by lime<br>and seawater                    | 3.10       |
| CHEMFE - Chemical precipitation by<br>FeCl <sub>3</sub> *6H <sub>2</sub> O | 3.14       |
| MIX - A mixing device  | 3.18       |
| PRESLU - Preliminary sludge treatment                                      | 3.22       |
| PREWAT - Preliminary water treatment                                       | 3.26       |
| PRISED - Primary sedimentation   | 3.30       |
| SPLIT - A splitting device   | 3.34       |
| STAAER - Aerobic sludge stabilization                                      | 3.38       |
| STALIM - Lime stabilization of sludge                                      | 3.42       |
| THICK - Sludge thickening  | 3.46       |
| 4. SYSTEM DESCRIPTION  | 4.1 - 4.12 |
| 4.1 Plot   | 4.2        |
| 4.2 Print  | 4.2        |
| 4.3 Display  | 4.7        |
| 4.4 Process description  | 4.10       |
| 4.5 Input wastewater characterization                                      | 4.12       |
| 4.6 Iteration  | 4.12       |
| 5. COMPLETE EXAMPLE  | 5.1 - 5.57 |
| 6. REFERENCES  | 6.1        |

## 1. OBJECTIVES FOR PROGRAM DEVELOPMENT

The model program PREDES (Preliminary Design of Wastewater Treatment Systems) is developed to fulfill the following objectives:

- mass balance calculations for treatment plants, based on a steady state condition for continuously working treatment processes
- calculation of dimensions for the different process units, based on design criteria given by the user

Another objective has been to make the program system flexible and self-explaining; i.e. develop an interactive program version.

## 2. SPECIAL CHARACTERISTICS

### 2.1 Flow chart

For each treatment process configuration, the user has to specify the flow chart for the system. Also recycling streams from sludge treatment processes can be considered.

The processes and the sludge and water streams should be assigned numbers for identification, as shown in the example in pt. 5.

### 2.2 Design flow rates

The design flow rates for a treatment plant are given in the form recommended by the Norwegian guidelines for design of wastewater treatment plants. According to this recommendation, two flow rates are necessary:

- a) Design flow rate  $Q_{dim}$  (m<sup>3</sup>/h)
- b) Maximum design flow rate  $Q_{maxdim}$  (m<sup>3</sup>/h)

These flow rates can be given explicitly, or calculated from the following formulae:

- c)  $Q_{dim} = q_s * P / T_s + q_i * P / 24 + Q_{ind} / T_{ind}$  (m<sup>3</sup>/h)
- d)  $Q_{maxdim} = f * Q_{dim}$  (m<sup>3</sup>/h)

where

- $q_s$  = mean sewage flow per capita per day (m<sup>3</sup>/cap/day)
- $q_i$  = mean infiltration flow per capita per day (m<sup>3</sup>/cap/day)
- $Q_{ind}$  = industrial wastewater flow per day (m<sup>3</sup>/day)
- $P$  = person equivalents connected to the plant (cap)
- $T_s$  = hours, over which the sewage flow is distributed (h)

If  $T_s$  is not given explicitly, it will be calculated from

$$T_s = 24. / (1. + 31.5 / \sqrt{P})$$

- $T_{ind}$  = number of hours, over which the industrial flow is distributed (h)
- $f$  = multiplier, giving the ratio  $Q_{maxdim} / Q_{dim}$  (h)

All the water treatment processes are designed according to the values for  $Q_{dim}$  and  $Q_{maxdim}$ . Sludge treatment processes are designed partly based on values from the mass balance calculations.

### 2.3 Stream characteristics

Each of the sludge and water streams are characterized by the following parameters;

| Flow rate                 | m <sup>3</sup> /h | Q           |           |
|---------------------------|-------------------|-------------|-----------|
| Concentrations of         |                   | Fraction    |           |
|                           |                   | Particulate | Dissolved |
| Suspended solids          | kg/m <sup>3</sup> | SS/P        |           |
| Volatile susp. solids     | kg/m <sup>3</sup> | VSS/P       |           |
| Biochemical oxygen demand | kg/m <sup>3</sup> | BOF7/P      | BOF7/D    |
| Phosphorus                | kg/m <sup>3</sup> | P/P         | P/D       |
| Nitrogen                  | kg/m <sup>3</sup> | N/P         | N/D       |
| Cadmium                   | g/m <sup>3</sup>  | CD/P        | CD/D      |
| Mercury                   | g/m <sup>3</sup>  | HG/P        | HG/D      |
| Lead                      | g/m <sup>3</sup>  | PB/P        | PB/D      |
| Calcium                   | kg/m <sup>3</sup> | CA/P        | CA/D      |
| Magnesium                 | kg/m <sup>3</sup> | MG/P        | MG/D      |
| Alkalinity                | eq/m <sup>3</sup> |             | ALK/D     |
| pH                        |                   |             | PH/D      |

#### SPECIAL PARAMETERS FOR SLUDGE;

|                  |        |         |
|------------------|--------|---------|
| Hygiene          | 0 - 10 | HYGIENE |
| Odor             | 0 - 10 | ODOR    |
| Plant protection | 0 - 10 | PPROT   |

The special parameters are assigned to the sludge streams on a subjective scale, ranging from 0 to 10. The index 10 is used for the least satisfactory quality. Increased quality is indicated by a decreasing index number.

For the water treatment processes, the special sludge quality indexes are given as default values by the program, as follows;

|                        | Hygiene | Odor | Plant protec. |
|------------------------|---------|------|---------------|
| Primary sedimentation  | 8.      | 8.   | 8.            |
| Chemical precipitation |         |      |               |
| Alum                   | 5.      | 5.   | 7.            |
| FeCl <sub>3</sub>      | 5.      | 5.   | 7.            |
| Lime                   | 3.      | 3.   | 5.            |

Sludge quality indexes should be given explicitly for external sludge input.

For the sludge treatment processes, the changes in quality indexes are given as per cent improvement (reduction). The default values given in the program:

|                       | Per cent reduction |      |             |
|-----------------------|--------------------|------|-------------|
|                       | Hygiene            | Odor | Plant prot. |
| Preliminary treatment | 0.0                | 0.0  | 0.0         |
| Sludge thickening     | 0.0                | 0.0  | 0.0         |
| Sludge dewatering     | 0.0                | 0.0  | 0.0         |
| Stabilization         |                    |      |             |
| Aerobic               | 40.0               | 90.0 | 10.0        |
| Lime                  | 80.0               | 20.0 | 20.0        |

### 3. PROCESS DESCRIPTION

The following unit processes are implemented in the 1. version of the program PREDES;

#### Water treatment

- PREWAT - Preliminary treatment
- PRISED - Primary sedimentation
- CHEMAL - Chemical precipitation/alum
- CHEMFE - Chemical precipitation/Fe(III)
- CHEMCA - Chemical precipitation/lime and seawater

#### Sludge treatment

- PRESLU - Preliminary treatment of external sludge
- THICK - Gravity thickening
- STAAER - Aerobic sludge stabilization
- STALIM - Lime stabilization
- CENTRI - Sludge dewatering

#### Combined processes

- MIX - A mixing device
- SPLIT - A splitting device

As seen from the list, biological water treatment processes are not implemented in this 1. program version. For sludge treatment options, sludge holding tanks, anaerobic stabilization, conditioning and the composting process are not implemented.

The conditioning process is implicitly taken care of by the users control of the dewatering process CENTRI. The composting process itself do not interfere with the treatment process by producing sludge water for recycling, and hence do not cause any treatment problems.

As the system configuration is, processes can be added or deleted in a simple way.

On the following pages, each of the treatment processes is described in alphabetic order. For the user's benefit, an instructive example is shown for each of them.



## Process Identification

P R O C E S S

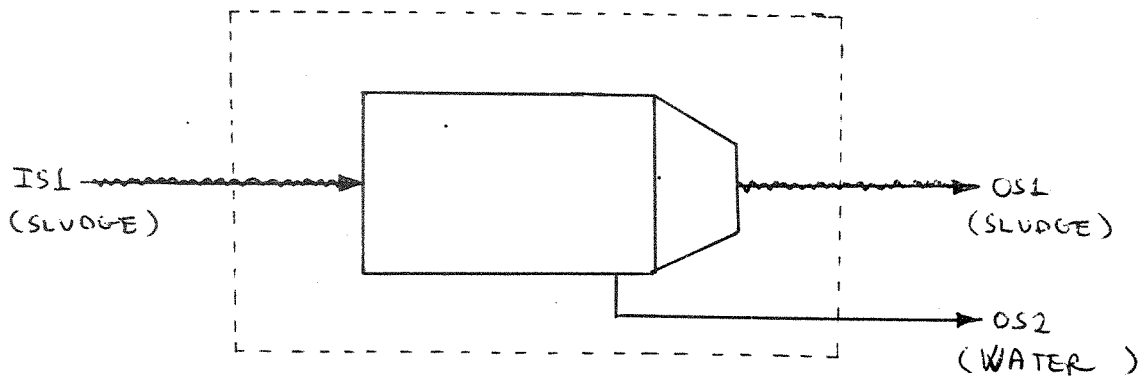
**Centri**

PROCESS NAME: SLUDGE DEWATERING - CENTRIFUGATION

## Process Description

A dewatering process, in which the suspended solids concentration in the sludge stream are considerably increased.

### Process Sketch



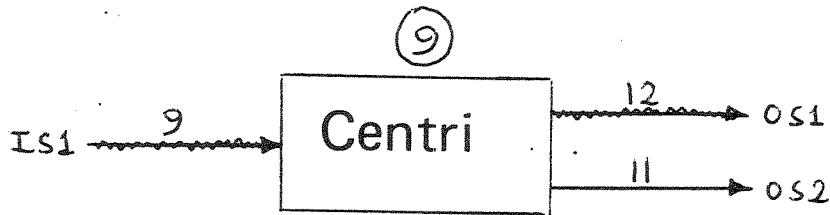
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : SLUDGE INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : ———  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : SLUDGE OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : WATER OUTPUT

### Process Characteristics

| Name   | Unit                 | Option |
|--|----------------------|--------|
| SOLIDS RECOVERY RATIO FOR CENTRIFUGATION               |                      | M1 (1) |
| SUSPENDED SOLIDS CONCENTRATION OF SLUDGE OUTPUT STREAM | (KG/M <sup>3</sup> ) | M2 (2) |

### Specification Example



=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 9 ↵  
PROCESS NAME : CENTRI ↵

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ↵

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 9 ↵  
SECOND INPUT STREAM NUMBER (IS2) : 0 ↵  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 12 ↵  
SECOND OUTPUT STREAM NUMBER (OS2) : 11 ↵

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ↵

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: CENTRI

SOLIDS RECOVERY RATIO FOR CENTRIFUGATION : 0.95 ↵  
SUSPENDED SOLIDS CONCENTRATION OF SLUDGE :  
OUTPUT STREAM (KG/M3) : 200 ↵

=====  
E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. No changes in the concentrations of dissolved matter.
2. Particulate matter concentrations in the output streams are proportional to the suspended solids concentrations.
3. Different specific gravity in the output streams are not accounted for.

### B. MODEL PRINCIPLES

1. Dissolved matter concentrations: Output=Input
2. Particulate matter:
  - a) A mass balance on suspended solids, giving the flow rates for the water effluent and the sludge stream.
  - b) The concentrations of the constituents connected to suspended solids are calculated from mass balances, in which the principle of homogeneous mixing are applied.
3. Special parameters for sludge quality in the output sludge stream are set equal to the input values.

Process Identification

P R O C E S S

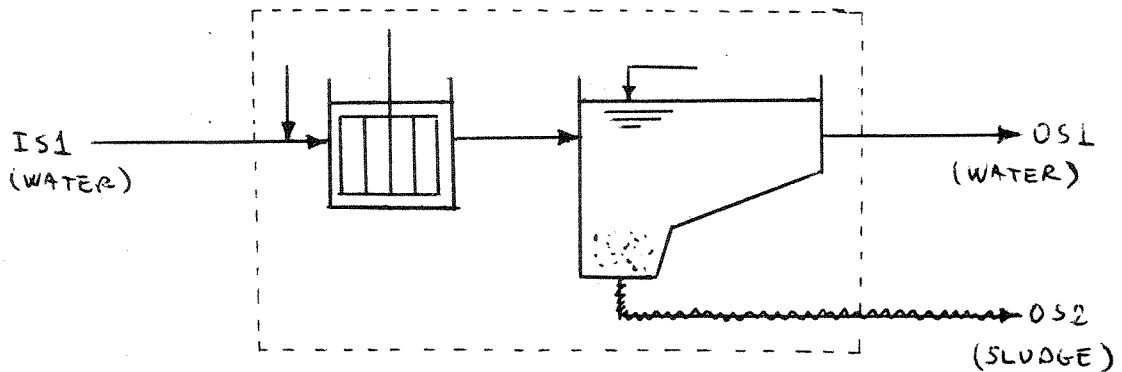
Chemal

PROCESS NAME: CHEMICAL PRECIPITATION BY ALUM

Process Description

Chemical precipitation by alum,  $Al_2(SO_4)_3 \cdot 18H_2O$ , including chemical addition, coagulation, flocculation and gravity sedimentation.

### Process Sketch



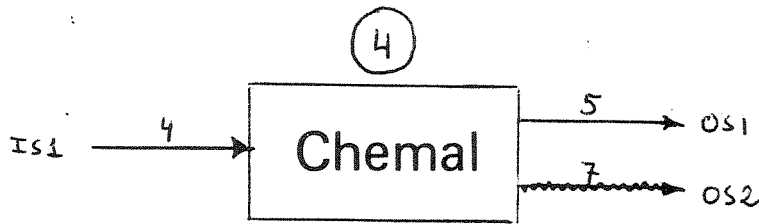
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : ———  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : SLUDGE OUTPUT

### Process Characteristics

| Name                             | UNIT                                | Option    |
|----------------------------------|-------------------------------------|-----------|
| CHEMICAL ADDITION                |                                     |           |
| PRECIPITATION PH                 |                                     | M1-A (1)  |
| DOSE OF ALUM                     | (G/M <sup>3</sup> )                 | M1-B (2)  |
| RATIO AL/TOT-P                   | (MOL/MOL)                           | M1-C (3)  |
| * FLOCCULATION                   |                                     |           |
| TEMPERATURE                      | (DEG C)                             | M2 (4)    |
| NUMBER OF CHAMBERS               |                                     | M3 (5)    |
| TOTAL DETENTION TIME AT QDIM     | (MIN)                               | M4 (6)    |
| * SEDIMENTATION BASIN            |                                     |           |
| OVERFLOW RATE AT QDIM            | (M <sup>3</sup> /M <sup>2</sup> /H) | M5-A (7)  |
| AT QMAXDIM                       | (M <sup>3</sup> /M <sup>2</sup> /H) | M5-A (8)  |
| TOTAL AREA                       | ((10**3)*M2)                        | M5-B (9)  |
| DETENTION TIME AT QDIM           | (H)                                 | M6-A (10) |
| DEPTH                            | (M)                                 | M6-B (11) |
| VOLUME                           | ((10**3)*M3)                        | M6-C (12) |
| SUSPENDED SOLIDS CONCENTRATIONS: |                                     |           |
| WATER EFFLUENT (WHEN PREFIXED)   | (KG/M <sup>3</sup> )                | M7 (13)   |
| CHEMICAL SLUDGE                  | (KG/M <sup>3</sup> )                | M8 (14)   |

## Specification Example



===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 4 ↘  
 PROCESS NAME : CHEMAL ↘

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ↘

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 4 ↘  
 SECOND INPUT STREAM NUMBER (IS2) : 0 ↘  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 5 ↘  
 SECOND OUTPUT STREAM NUMBER (OS2) : 7 ↘

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ↘

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: CHEMAL

\* CHEMICAL ADDITION  
 PRECIPITATION PH : 5.7 ↘

\* FLOCCULATION  
 TEMPERATURE (DEG C) : 10. ↘  
 NUMBER OF CHAMBERS : 3. ↘  
 TOTAL DETENTION TIME AT QDIM (MIN) : 30. ↘

\* SEDIMENTATION BASIN  
 OVERFLOW RATE AT QDIM (M3/M2/H) : 1.3 ↘  
 AT QMAXDIM (M3/M2/H) : 2.0 ↘  
 DETENTION TIME AT QDIM (H) : 2 ↘  
 DEPTH (M) : 2.5 ↘

SUSPENDED SOLIDS CONCENTRATIONS:  
 WATER EFFLUENT (WHEN PREFIXED) (KG/M3) : 0.015 ↘  
 CHEMICAL SLUDGE (KG/M3) : 7.5 ↘

===== E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. The precipitation products are the inorganic components  $AlPO_4$  and  $Al(OH)_3$ .
2. For the given suspended solids concentration in the output streams, the concentrations of other particulate constituents are calculated proportional to suspended solids.
3. The change in specific gravity in the sludge stream are not accounted for.
4. The dissolved matter concentrations in the water effluent are fixed to a given percentage of influent concentrations.

### B. MODEL PRINCIPLES

1. The precipitation process is based on pH and alkalinity, as follows:
  - a) Intermediate pH and alkalinity, resulting from  $AlPO_4$ -precipitation.
  - b) Final pH and alkalinity after  $Al(OH)_3$ -precipitation.
2. Concentration changes of dissolved matter are calculated for the following constituents only, for which the fractional removal (normal municipal wastewater assumed) are fixed to:

P/D = 0.95  
CD/D = 0.95  
HG/D = 0.50  
PB/D = 0.95

3. Particulate matter concentrations are based on mass balances.
4. Special parameters for sludge quality are fixed as follows:

HYGIENE : 5.  
ODOR : 5.  
PPROT : 7.



## Process Identification

P R O C E S S

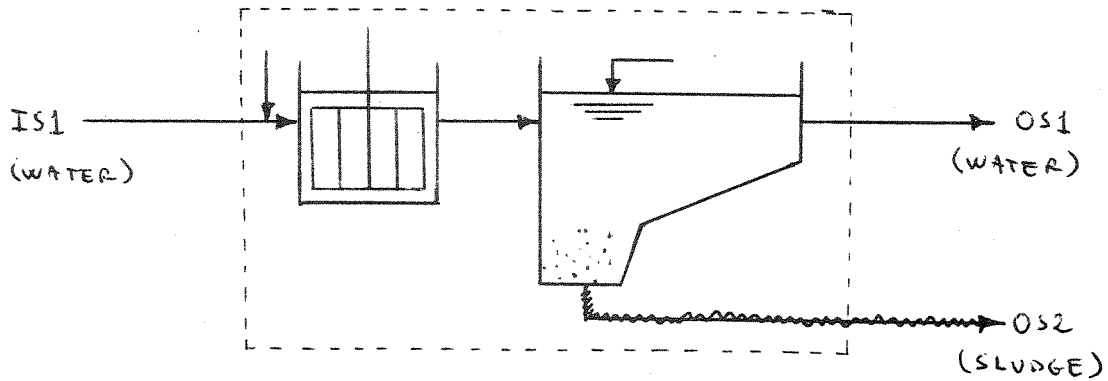
**Chemca**

PROCESS NAME: CHEMICAL PRECIPITATION BY LIME AND SEAWATER

## Process Description

Chemical precipitation by  $\text{Ca}(\text{OH})_2$ , or by  $\text{Ca}(\text{OH})_2$  and seawater addition. The process includes addition of chemicals (and seawater), coagulation, flocculation and gravity sedimentation.

### Process Sketch



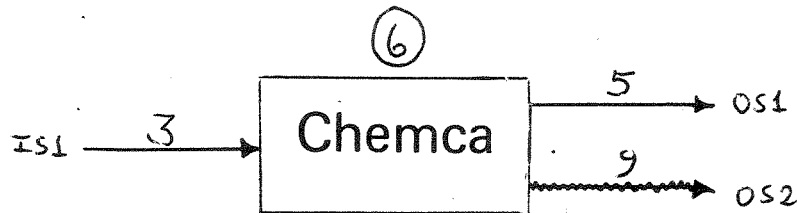
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : \_\_\_\_\_  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : SLUDGE OUTPUT

### Process Characteristics

| Name                             | Unit                                | Option    |
|----------------------------------|-------------------------------------|-----------|
| * CHEMICAL ADDITION              |                                     |           |
| PRECIPITATION PH                 |                                     | M1 (1)    |
| DOSE OF CA(OH) <sub>2</sub>      | (G/M <sup>3</sup> )                 | M2 (2)    |
| VOLUME FRACTION SEAWATER/INFLOW  | (%)                                 | M3-A (3)  |
| SEAWATER SALINITY                | (PP.MILL)                           | M3-A (4)  |
| * FLOCCULATION                   |                                     |           |
| TEMPERATURE                      | (DEG C)                             | M4 (5)    |
| NUMBER OF CHAMBERS               |                                     | M5 (6)    |
| TOTAL DETENTION TIME AT QDIM     | (MIN)                               | M6 (7)    |
| * SEDIMENTATION BASIN            |                                     |           |
| OVERFLOW RATE AT QDIM            | (M <sup>3</sup> /M <sup>2</sup> /H) | M7-A (8)  |
| AT QMAXDIM                       | (M <sup>3</sup> /M <sup>2</sup> /H) | M7-A (9)  |
| TOTAL AREA                       | ((10**3)*M <sup>2</sup> )           | M7-B (10) |
| DETENTION TIME AT QDIM           | (H)                                 | M8-A (11) |
| DEPTH                            | (M)                                 | M8-B (12) |
| VOLUME                           | ((10**3)*M <sup>3</sup> )           | M8-C (13) |
| SUSPENDED SOLIDS CONCENTRATIONS: |                                     |           |
| WATER EFFLUENT (WHEN PREFIXED)   | (KG/M <sup>3</sup> )                | M9 (14)   |
| CHEMICAL SLUDGE                  | (KG/M <sup>3</sup> )                | M10 (15)  |

## Specification Example

=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 6  
 PROCESS NAME : CHEMCA

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 3  
 SECOND INPUT STREAM NUMBER (IS2) : 0  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 5  
 SECOND OUTPUT STREAM NUMBER (OS2) : 9

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: CHEMCA

## \* CHEMICAL ADDITION

PRECIPITATION PH : 11.4  
 DOSE OF CA(OH)<sub>2</sub> (G/M<sup>3</sup>) : 2  
 VOLUME FRACTION SEAWATER/INFLOW (%) : 5  
 SEAWATER SALINITY (PR.MILL) : 30

## \* FLOCCULATION

TEMPERATURE (DEG C) : 13  
 NUMBER OF CHAMBERS : 4  
 TOTAL DETENTION TIME AT QDIM (MIN) : 15

## \* SEDIMENTATION BASIN

OVERFLOW RATE AT QDIM (M<sup>3</sup>/M<sup>2</sup>/H) : 1.6  
 AT QMAXDIM (M<sup>3</sup>/M<sup>2</sup>/H) : 2.4  
 DETENTION TIME AT QDIM (H) :  
 DEPTH (M) : 2.5

## SUSPENDED SOLIDS CONCENTRATIONS:

WATER EFFLUENT (WHEN PREFIXED) (KG/M<sup>3</sup>) : 0.025  
 CHEMICAL SLUDGE (KG/M<sup>3</sup>) : 50

=====  
E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. The precipitation products are the inorganic components  $\text{Ca}_{10}(\text{PO}_4)_6 \cdot (\text{OH})_2$ ,  $\text{M}_s(\text{OH})_2$  and  $\text{CaCO}_3$ .
2. For given suspended solids concentrations in the output streams, the concentrations of other particulate constituents are calculated proportional to suspended solids.
3. The change in specific gravity in the sludge stream is not accounted for.
4. The dissolved matter concentrations in the water effluent are fixed to a given percentage of the influent concentrations.

### B. MODEL PRINCIPLES

1. The theoretical necessary dose of  $\text{Ca}(\text{OH})_2$  to obtain the given precipitation pH are calculated from:
  - a) increase in concentration of free OH-ions
  - b) displacement of equilibrium in the carbonate system
  - c) displacement of equilibrium in the system  $\text{NH}_4 - \text{NH}_3$
  - d) displacement of equilibrium of phosphates
  - e) precipitation of  $\text{Ca}_{10}(\text{PO}_4)_6 \cdot (\text{OH})_2$
  - f) precipitation of  $\text{M}_s(\text{OH})_2$
2. The precipitation of  $\text{CaCO}_3$  is based on an equilibrium around the Ca-ion.
3. If the actual dose of  $\text{Ca}(\text{OH})_2$  exceeds the theoretical dose calculated in B1, the difference is accounted for in the sludge production as unused lime.
4. Concentration changes of dissolved matter are calculated for the following constituents only, for which the fractional removal (normal municipal wastewater assumed) are fixed to:

F/D = 0.95  
CD/D = 0.95  
HG/D = 0.50  
PB/D = 0.95

5. Particulate matter concentrations are based on mass balances.
6. Special parameters for sludge quality are fixed as follows:

HYGIENE : 3.  
ODOR : 3.  
PPROT : 5.

## Process Identification

P P O C E S S

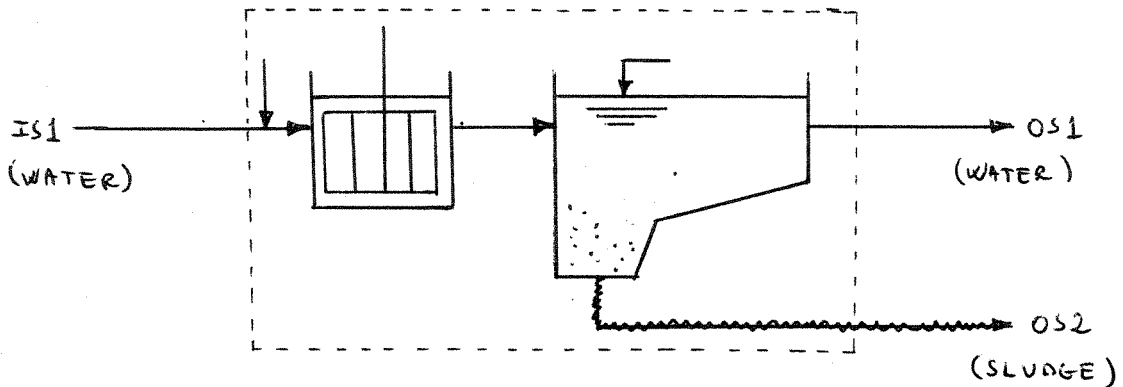
**Chemfe**

PROCESS NAME: CHEMICAL PRECIPITATION BY  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$

## Process Description

Chemical precipitation by  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , including chemical addition, coagulation, flocculation and gravity sedimentation.

### Process Sketch



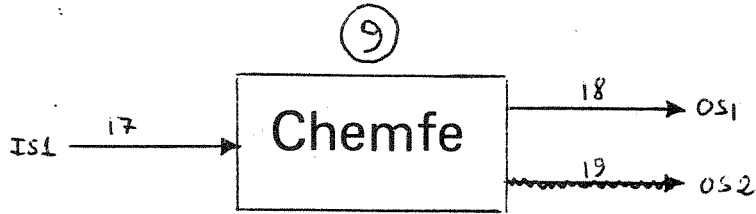
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : \_\_\_\_\_  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : SLUDGE OUTPUT

### Process Characteristics

| Name                             | Unit         | Option      |
|----------------------------------|--------------|-------------|
| * CHEMICAL ADDITION              |              |             |
| PRECIPITATION PH                 |              | M1 - A (1)  |
| DOSE OF FECL3*6H2O               | (G/M3)       | M1 - B (2)  |
| RATIO FE/TOT-F                   | (MOL/MOL)    | M1 - C (3)  |
| * FLOCCULATION                   |              |             |
| TEMPERATURE                      | (DEG C)      | M2 (4)      |
| NUMBER OF CHAMBERS               |              | M3 (5)      |
| TOTAL DETENTION TIME AT QDIM     | (MIN)        | M4 (6)      |
| * SEDIMENTATION BASIN            |              |             |
| OVERFLOW RATE AT QDIM            | (M3/M2/H)    | M5 - A (7)  |
| AT QMAXDIM                       | (M3/M2/H)    | M5 - A (8)  |
| TOTAL AREA                       | ((10**3)*M2) | M5 - B (9)  |
| DETENTION TIME AT QDIM           | (H)          | M6 - A (10) |
| DEPTH                            | (M)          | M6 - B (11) |
| VOLUME                           | ((10**3)*M3) | M6 - C (12) |
| SUSPENDED SOLIDS CONCENTRATIONS: |              |             |
| WATER EFFLUENT (WHEN PREFIXED)   | (KG/M3)      | M7 (13)     |
| CHEMICAL SLUDGE                  |              | M8 (14)     |

## Specification Example



===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 9  
 PROCESS NAME : CHEMFE

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 17  
 SECOND INPUT STREAM NUMBER (IS2) : 0  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 18  
 SECOND OUTPUT STREAM NUMBER (OS2) : 19

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: CHEMFE

\* CHEMICAL ADDITION  
 PRECIPITATION PH : 5.0

\* FLOCCULATION  
 TEMPERATURE (DEG C) : 10  
 NUMBER OF CHAMBERS : 3  
 TOTAL DETENTION TIME AT QDIM (MIN) : 30

\* SEDIMENTATION BASIN  
 OVERFLOW RATE AT QDIM (M3/M2/H) : 1.3  
 AT QMAXDIM (M3/M2/H) : 2.0  
 DETENTION TIME AT QDIM (H) : 2  
 DEPTH (M) : 2.5

SUSPENDED SOLIDS CONCENTRATIONS:  
 WATER EFFLUENT (WHEN PREFIXED) (KG/M3) : 0.020  
 CHEMICAL SLUDGE (KG/M3) : 7.5

===== E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. The precipitation products are the inorganic components  $\text{FePO}_4$  and  $\text{Fe}(\text{OH})_3$ .
2. For the given suspended solids concentration in the output streams, the concentrations of other particulate constituents are calculated proportional to suspended solids.
3. The change in specific gravity in the sludge stream are not accounted for.
4. The dissolved matter concentrations in the water effluent are fixed to a given per centage of influent concentrations.

### B. MODEL PRINCIPLES

1. The precipitation process is based on pH and alkalinity, as follows:
  - a) Intermediate pH and alkalinity, resulting from  $\text{FePO}_4$ -precipitation.
  - b) Final pH and alkalinity after  $\text{Fe}(\text{OH})_3$ -precipitation.
2. Concentration changes of dissolved matter are calculated for the following constituents only, for which the fractional removal (normal municipal wastewater assumed) are fixed to:

$$\begin{aligned} \text{F/D} &= 0.95 \\ \text{CD/D} &= 0.95 \\ \text{HG/D} &= 0.50 \\ \text{PB/D} &= 0.95 \end{aligned}$$

3. Particulate matter concentrations are based on mass balances.
4. Special parameters for sludge quality are fixed as follows:

$$\begin{aligned} \text{HYGIENE} &: 5. \\ \text{ODOR} &: 5. \\ \text{P\%ROT} &: 7. \end{aligned}$$



## Process Identification

P R O C E S S

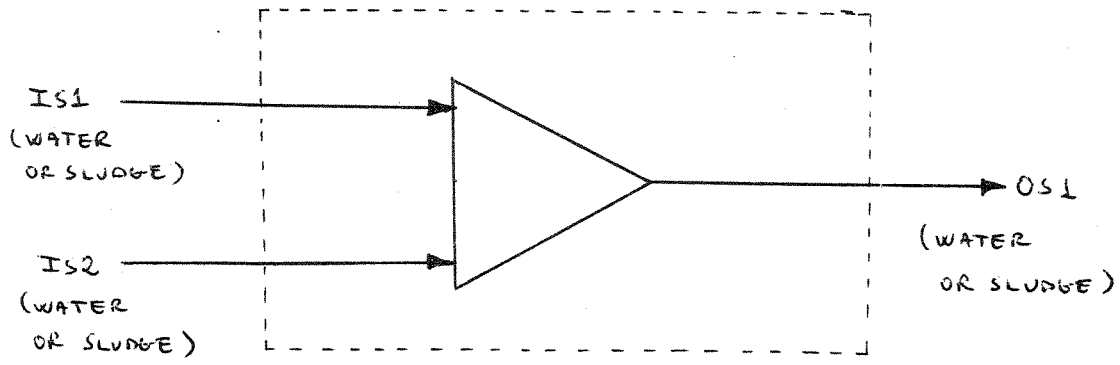
**Mix**

PROCESS NAME: STREAM MIXER

## Process Description

A mixing device, in which two separate streams are mixed into a single output stream.

### Process Sketch



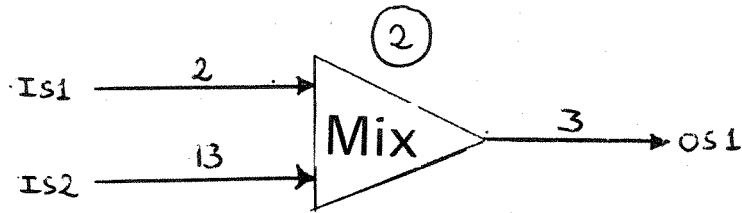
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER OR SLUDGE INPUT  
SECOND INPUT STREAM NUMBER (IS2) : WATER OR SLUDGE INPUT  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OR SLUDGE OUTPUT  
SECOND OUTPUT STREAM NUMBER (OS2) : \_\_\_\_\_

### Process Characteristics

| Name | Unit | Option |
|------|------|--------|
|------|------|--------|

## Specification Example



===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 2  
 PROCESS NAME : MIX

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 2  
 SECOND INPUT STREAM NUMBER (IS2) : 13  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 3  
 SECOND OUTPUT STREAM NUMBER (OS2) : 0

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: MIX

===== E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. The mixing process is complete
2. If the input streams have different specific gravity, this is not accounted for in the flow rate calculations.

### B. MODEL PRINCIPLES

1. Flow continuity, setting the flow rate of the output stream equal to the sum of the input streams.
2. The concentrations in the output stream are calculated based on a mass balance principle.
3. If sludges with different quality indexes for hygiene, odor and plant protection are mixed, the output indexes are calculated on a mass balance principle, according to 2.

Process Identification

P R O C E S S

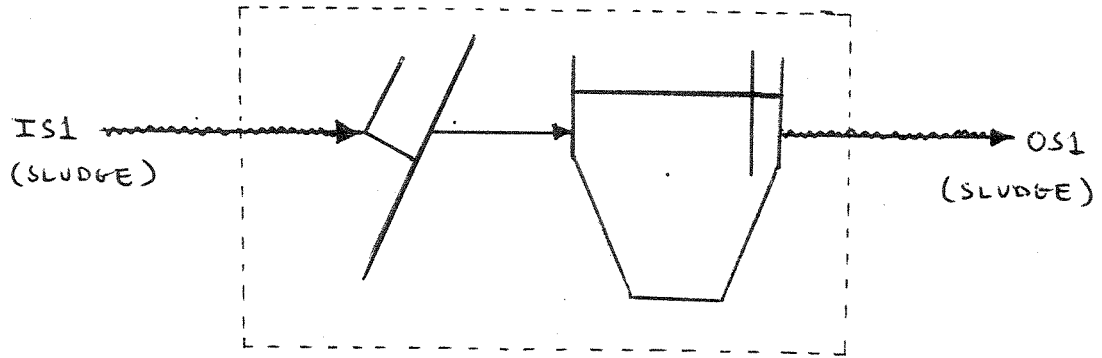
Preslu

PROCESS NAME: PRELIMINARY TREATMENT OF SLUDGE

Process Description

Preliminary sludge treatment processes, including physical unit operations as bar screenings and grit removal.

### Process Sketch



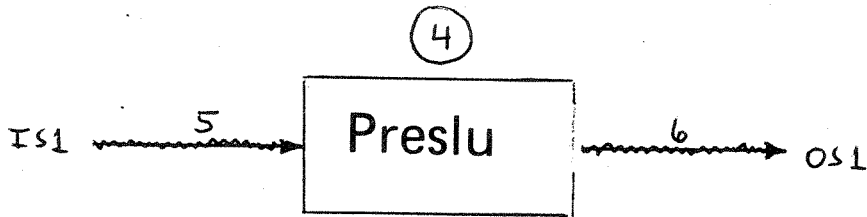
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : SLUDGE INPUT  
SECOND INPUT STREAM NUMBER (IS2) : \_\_\_\_\_  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : SLUDGE OUTPUT  
SECOND OUTPUT STREAM NUMBER (OS2) : \_\_\_\_\_

### Process Characteristics

| Name | Unit | Option |
|------|------|--------|
|------|------|--------|

## Specification Example

=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 4 ↘  
 PROCESS NAME : PRESLU ↘

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ↘

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 5 ↘  
 SECOND INPUT STREAM NUMBER (IS2) : 0 ↘  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 6 ↘  
 SECOND OUTPUT STREAM NUMBER (OS2) : 0 ↘

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ↘

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: PRESLU

=====  
E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. No changes in the concentrations of dissolved matter in the processes.
2. No changes in the concentrations of suspended matter.

### B. MODEL PRINCIPLE

1. Output = Input



Process Identification

P R O C E S S

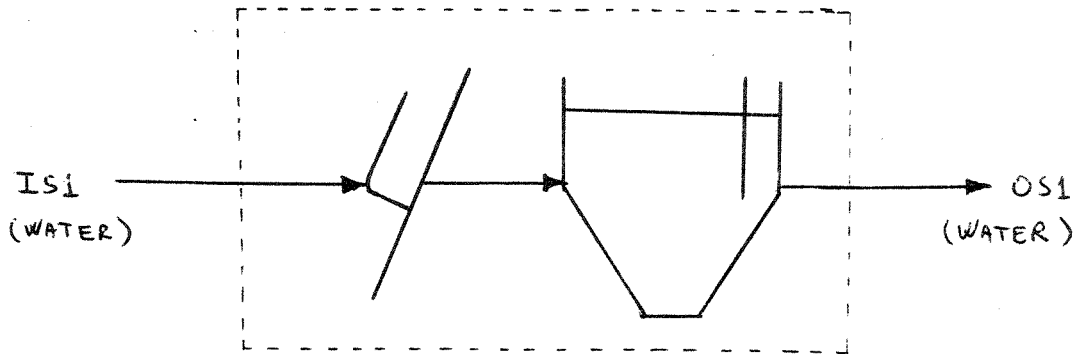
Prewat

PROCESS NAME: PRELIMINARY TREATMENT OF WATER

Process Description

Preliminary water treatment processes, including physical unit operations as bar screening and grit removal.

### Process Sketch



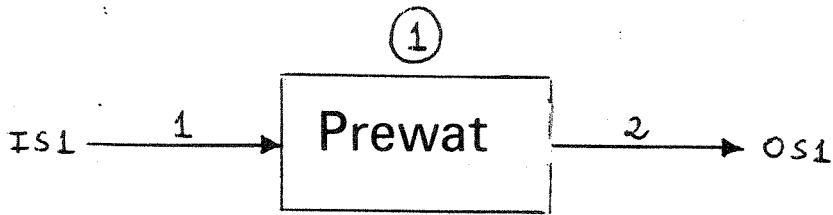
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER INPUT  
SECOND INPUT STREAM NUMBER (IS2) : \_\_\_\_\_  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OUTPUT  
SECOND OUTPUT STREAM NUMBER (OS2) : \_\_\_\_\_

### Process Characteristics

| Name | Unit | Option |
|------|------|--------|
|------|------|--------|

### Specification Example



=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 1  
PROCESS NAME : PREWAT

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 1  
SECOND INPUT STREAM NUMBER (IS2) : 0  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 2  
SECOND OUTPUT STREAM NUMBER (OS2) : 0

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: PREWAT

=====  
E N D C H A R A C T E R I S T I C S

## Process Model

---

### A. ASSUMPTIONS

1. No changes in the concentrations of dissolved matter in the processes.
2. No changes in the concentrations of suspended matter.

### B. MODEL PRINCIPLE

1. Output = Input

## Process Identification

P R O C E S S

**Prised**

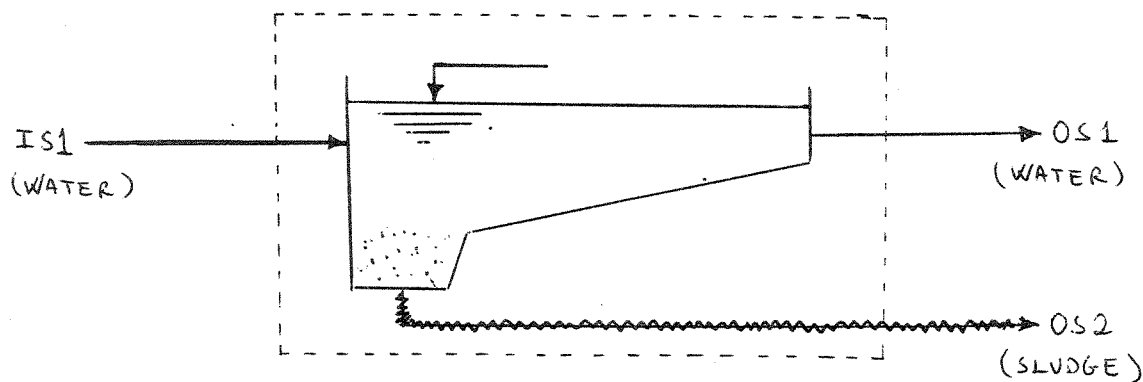
PROCESS NAME: PRIMARY SEDIMENTATION

## Process Description

Separation from water, by gravity settling, of suspended particles heavier than water.

The process routine does not include chemical addition. If primary precipitation is used, one of the chemical precipitation routines should be applied.

### Process Sketch



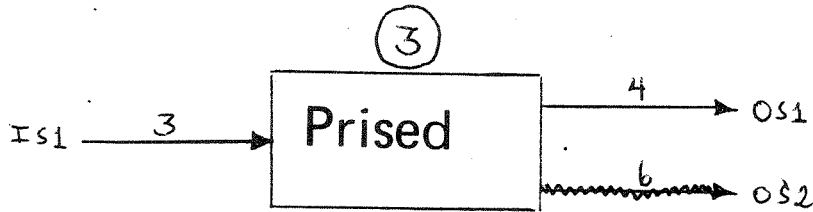
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : \_\_\_\_\_  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : SLUDGE OUTPUT

### Process Characteristics

| Name                             | Unit                                | Option   |
|----------------------------------|-------------------------------------|----------|
| * SEDIMENTATION BASIN            |                                     |          |
| OVERFLOW RATE AT QDIM            | (M <sup>3</sup> /M <sup>2</sup> /H) | M1-A (1) |
| AT QMAXDIM                       | (M <sup>3</sup> /M <sup>2</sup> /H) | M1-A (2) |
| TOTAL AREA                       | ((10**3)*M <sup>2</sup> )           | M1-B (3) |
| DETENTION TIME AT QDIM           | (H)                                 | M2-A (4) |
| DEPTH                            | (M)                                 | M2-B (5) |
| VOLUME                           | ((10**3)*M <sup>3</sup> )           | M2-C (6) |
| SUSPENDED SOLIDS CONCENTRATIONS: |                                     |          |
| WATER EFFLUENT (WHEN PREFIXED)   | (KG/M <sup>3</sup> )                | M3 (7)   |
| PRIMARY SLUDGE                   | (KG/M <sup>3</sup> )                | M4 (8)   |

### Specification Example



===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 3  
 PROCESS NAME : PRISED

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 3  
 SECOND INPUT STREAM NUMBER (IS2) : 0  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 4  
 SECOND OUTPUT STREAM NUMBER (OS2) : 6

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: PRISED

\* SEDIMENTATION BASIN

|                        |           |       |
|------------------------|-----------|-------|
| OVERFLOW RATE AT QDIM  | (M3/M2/H) | : 1.9 |
| AT QMAXDIM             | (M3/M2/H) | : 3.8 |
| RETENTION TIME AT QDIM | (H)       | : 5   |
| DEPTH                  | (M)       | : 2.5 |

SUSPENDED SOLIDS CONCENTRATIONS:

|                                |         |         |
|--------------------------------|---------|---------|
| WATER EFFLUENT (WHEN PREFIXED) | (KG/M3) | : 0.070 |
| PRIMARY SLUDGE                 | (KG/M3) | : 30.0  |

===== E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. No changes in the concentrations of dissolved matter in the process.
2. Particulate matter in the influent is removed proportional to the removal of suspended solids from the water.
3. The change in specific gravity in the sludge is not accounted for.

### B. MODEL PRINCIPLES

1. Dissolved matter: Output = Input
2. Particulate matter:
  - a) A mass balance on suspended solids, giving the flow rates
  - b) The concentrations of the constituents connected to suspended solids are calculated from mass balances, in which the principle of homogeneous mixing is applied.
3. Special parameters for sludge quality are fixed as follows:

HYGIENE : 8.  
ODOR : 8.  
PPROT : 8.



## Process Identification

P R O C E S S

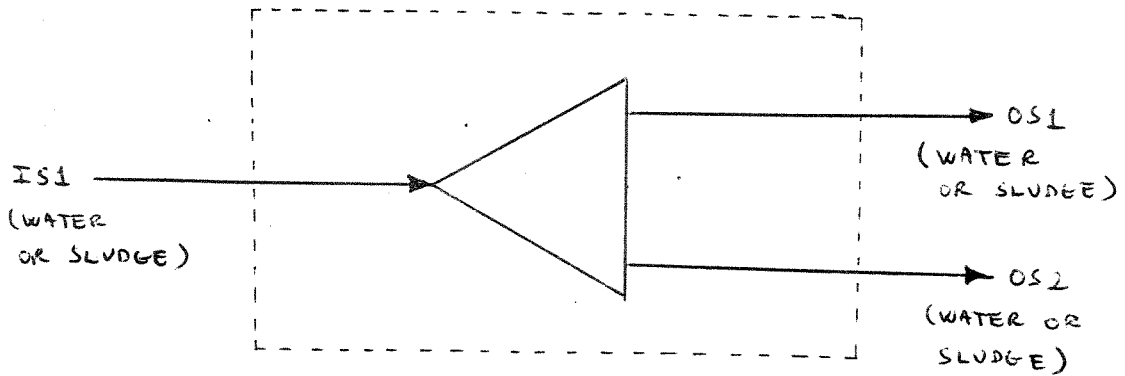
**Split**

PROCESS NAME:    STREAM SPLITTER

## Process Description

An overflow device, splitting a single stream into two separate streams.

### Process Sketch



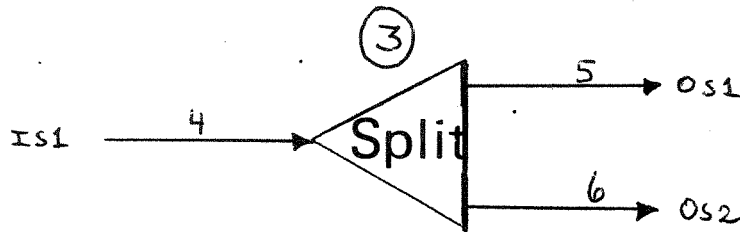
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : WATER OR SLUDGE INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : —  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : WATER OR SLUDGE OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : WATER OR SLUDGE OUTPUT

### Process Characteristics

| Name  | Unit                | Option |
|---|---------------------|--------|
| MAXIMUM FLOW OF PRINCIPAL OUTPUT STREAM (OS1) | (M <sup>3</sup> /H) | M1 (1) |

### Specification Example



===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 3  
 PROCESS NAME : SPLIT

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 4  
 SECOND INPUT STREAM NUMBER (IS2) : 0  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 5  
 SECOND OUTPUT STREAM NUMBER (OS2) : 6

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: SPLIT  
 MAXIMUM FLOW OF PRINCIPAL OUTPUT STREAM (OS1) (M3/H) : 5

===== E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. The principal output stream has a fixed upper hydraulic capacity limit.
2. Homogenous mixing in the splitter.

### B. MODEL PRINCIPLES

1. Flow continuity.

As long as the capacity of the principal output stream is not exceeded, the flow rate of the principal output stream is equal to the inflow rate.

When the input stream flow rate exceeds the principal output stream capacity, the difference is set equal to the flow rate of the second output stream.

2. The concentrations in the output streams are equal to the input concentrations.

## Process Identification

P R O C E S S

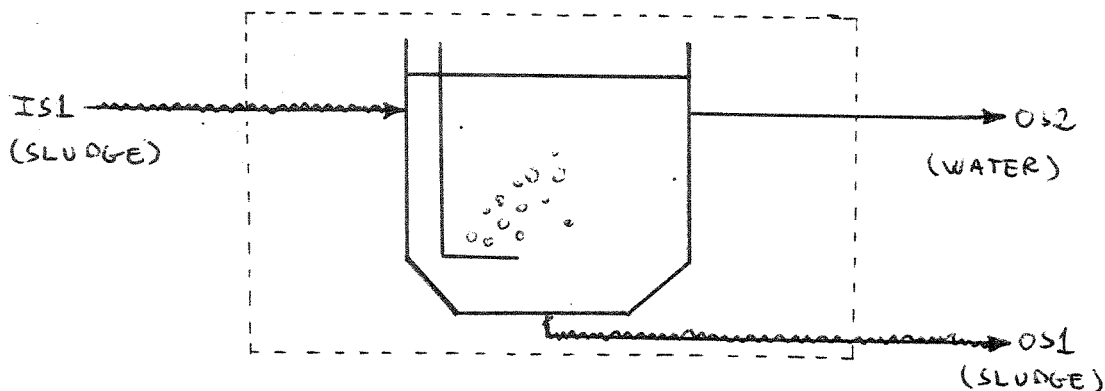
**Staaer**

PROCESS NAME: AEROBIC STABILIZATION OF SLUDGE

## Process Description

Stabilization of sludge under aerobic conditions.

### Process Sketch



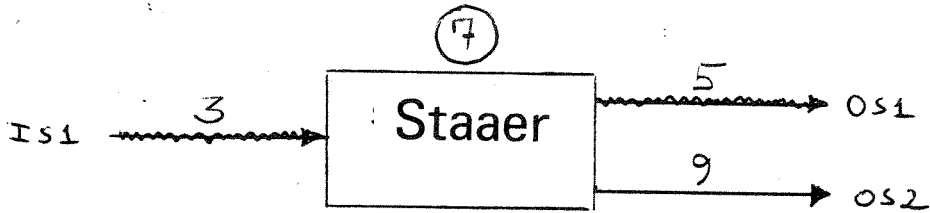
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : SLUDGE INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : ———  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : SLUDGE OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : WATER OUTPUT

### Process Characteristics

| Name   | Unit       | Option |
|--|------------|--------|
| SUSPENDED SOLIDS RETENTION TIME                        | (DAYS)     | M1 (1) |
| STABILIZATION TEMPERATURE                              | (DEG C)    | M2 (2) |
| SOLIDS RECOVERY RATIO FOR SLUDGE                       | (FRACTION) | M3 (3) |
| SUSPENDED SOLIDS CONCENTRATION OF SLUDGE OUTPUT STREAM | (KG/M**3)  | M4 (4) |

# Specification Example



===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 7  
 PROCESS NAME : STAAER

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 3  
 SECOND INPUT STREAM NUMBER (IS2) : 0  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 5  
 SECOND OUTPUT STREAM NUMBER (OS2) : 9

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: STAAER

|  |            |               |             |
|--|------------|---------------|-------------|
| SUSPENDED SOLIDS RETENTION TIME                        | (DAYS)     | : <u>20.</u>  | R<br>K<br>W |
| STABILIZATION TEMPERATURE                              | (DEG C)    | : <u>15.</u>  |             |
| SOLIDS RECOVERY RATIO FOR SLUDGE STREAM                | (FRACTION) | : <u>0.79</u> |             |
| SUSPENDED SOLIDS CONCENTRATION OF SLUDGE OUTPUT STREAM | (KG/M3)    | : <u>3.5</u>  |             |

===== E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. The stabilization process is not used in cases with lime precipitation.
2. Particulate matter concentrations in the output streams are proportional to the suspended solids concentrations.
3. Different specific gravity in the output streams are not accounted for.

### B. MODEL PRINCIPLES

1. The biological degradation of organic solid matter is assumed to follow a 1. order reaction;

$$(VSS_t - VSS_n)/(VSS_0 - VSS_n) = \exp(-Kt/t)$$

in which

VSS<sub>0</sub> = Volatile suspended solids concentration at time zero

VSS<sub>t</sub> = Volatile suspended solids concentration at time t

VSS<sub>n</sub> = Nonbiodegradable volatile suspended solids concentration, assumed to be 40 per cent of VSS<sub>0</sub>

t = detention time (days)

Kt = rate of decay (per day), assumed to be  $0.079 \times 1.10^{(T-20)}$ ;

T = temperature (deg C)

2. Soluble organic matter is assumed to follow the same decay rate as the solid organic matter.
3. Changes in pH and alkalinity are based on "black box"-modelling.
4. Other dissolved constituents are approximated to stay constant.
5. For the special sludge parameters, the following reductions are assumed;

|         |   |    |   |
|---------|---|----|---|
| Hysiene | - | 40 | % |
| Odor    | - | 90 | % |
| Plant   | - | 10 | % |



## Process Identification

P P O C E S S

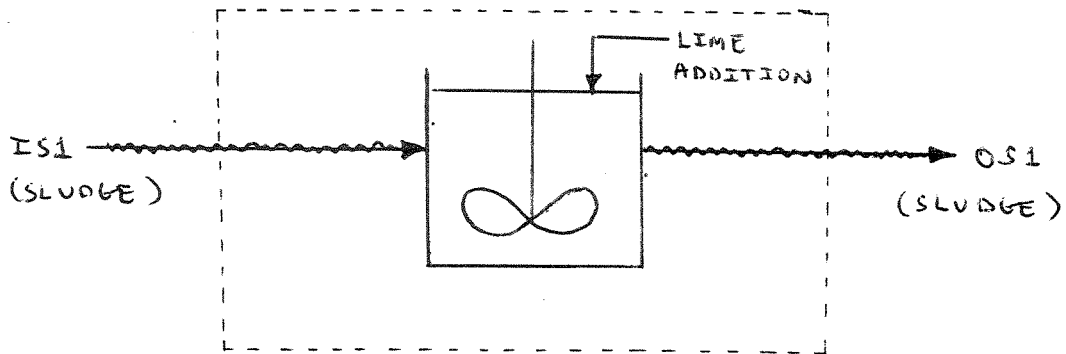
**Stalim**

PROCESS NAME: LIME STABILIZATION OF SLUDGE

## Process Description

A process, in which lime and sludge are mixed to produce a sludge, temporarily stabilized to inhibit biological degradation.

Process Sketch



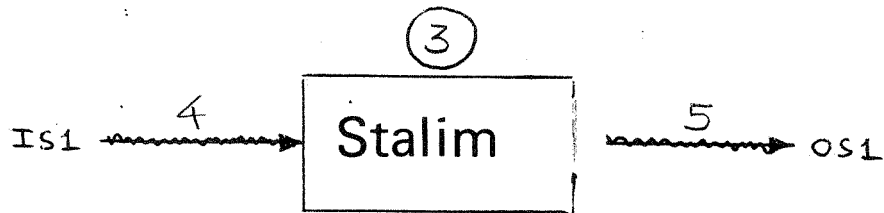
Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : SLUDGE INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : \_\_\_\_\_  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : SLUDGE OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : \_\_\_\_\_

Process Characteristics

| Name                          | <u>UNIT</u> | Option   |
|-------------------------------|-------------|----------|
| PH AFTER LIME ADDITION        | ( - )       | M1 - (1) |
| ACTUAL DOSE CA(OH)2           | (G/KG SS)   | M2 (2)   |
| TEMPERATURE                   | (DEG C)     | M3 (3)   |
| DETENTION TIME MIXING CHAMBER | (MIN)       | M4-A (4) |
| VOLUME OF MIXING CHAMBER      | (M**3)      | M4-B (5) |

## Specification Example



===== P R O C E S S IDENTIFICATION

PROCESS NUMBER (N) : 3 ✓  
 PROCESS NAME : STALIM ✓

===== E N D IDENTIFICATION

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ✓

===== P R O C E S S FLOW

PRINCIPAL INPUT STREAM NUMBER (IS1) : 4 ✓  
 SECOND INPUT STREAM NUMBER (IS2) : 0 ✓  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 5 ✓  
 SECOND OUTPUT STREAM NUMBER (OS2) : 0 ✓

===== E N D FLOW

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ✓

===== P R O C E S S CHARACTERISTICS

PROCESS NAME: STALIM

|                                   |           |                 |
|-----------------------------------|-----------|-----------------|
| PH AFTER LIME ADDITION            |           | : <u>11.6</u> ✓ |
| ACTUAL DOSE CA(OH) <sub>2</sub>   | (G/KG SS) | : <u>400.</u> ✓ |
| TEMPERATURE                       | (DEG C)   | : <u>13.</u> ✓  |
| DETENTION TIME FOR MIXING CHAMBER | (MIN.)    | : <u>10.</u> ✓  |

===== E N D CHARACTERISTICS

## Process Model

### A. ASSUMPTIONS

1. The precipitation products are the inorganic components  $\text{Ca}_{10}(\text{PO}_4)_6 \cdot (\text{OH})_2$ ,  $\text{Mg}(\text{OH})_2$  and  $\text{CaCO}_3$ .
2. For given suspended solids concentrations in the output streams, the concentrations of other particulate constituents are calculated proportional to suspended solids.
3. The change in specific gravity in the sludge stream is not accounted for.
4. The dissolved matter concentrations in the water effluent are fixed to a given percentage of the influent concentrations.

### B. MODEL PRINCIPLES

1. The theoretical necessary dose of  $\text{Ca}(\text{OH})_2$  to obtain the given precipitation pH are calculated from:
  - a) increase in concentration of free OH-ions
  - b) displacement of equilibrium in the carbonate system
  - c) displacement of equilibrium in the system  $\text{NH}_4 - \text{NH}_3$
  - d) displacement of equilibrium of phosphates
  - e) precipitation of  $\text{Ca}_{10}(\text{PO}_4)_6 \cdot (\text{OH})_2$
  - f) precipitation of  $\text{Mg}(\text{OH})_2$
2. The precipitation of  $\text{CaCO}_3$  is based on an equilibrium around the Ca-ion.
3. If the actual dose of  $\text{Ca}(\text{OH})_2$  exceeds the theoretical dose calculated in B1, the difference is accounted for in the sludge production as unused lime.
4. Concentration changes of dissolved matter are calculated for the following constituents only, for which the fractional removal (normal municipal wastewater assumed) are fixed to:

P/D = 0.95  
CB/D = 0.95  
HG/D = 0.50  
PB/D = 0.95

5. Particulate matter concentrations are based on mass balances.
6. Special parameters for sludge quality are fixed as follows:

HYGIENE : 3.  
ODOR : 3.  
PFPOT : 5.

## Process Identification

P R O C E S S

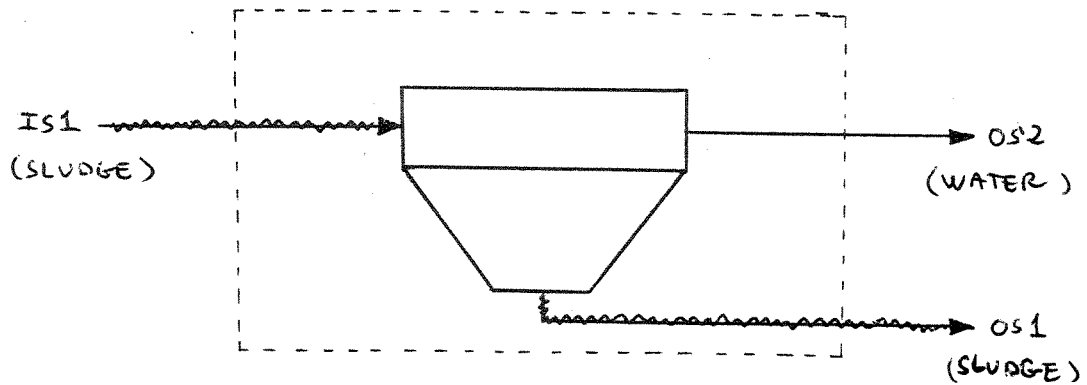
**Thick**

PROCESS NAME: SLUDGE THICKENING

## Process Description

Gravity thickening of sludge, giving a concentrated sludge stream and a water effluent.

### Process Sketch



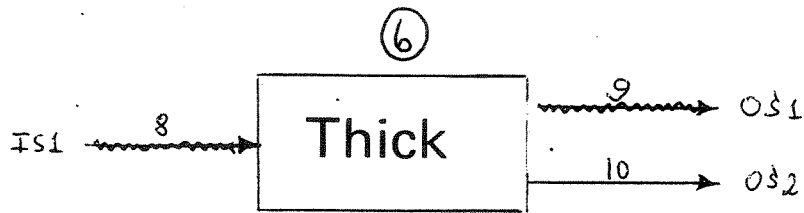
### Process Flows

PRINCIPAL INPUT STREAM NUMBER (IS1) : SLUDGE INPUT  
 SECOND INPUT STREAM NUMBER (IS2) : ———  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : SLUDGE OUTPUT  
 SECOND OUTPUT STREAM NUMBER (OS2) : WATER OUTPUT

### Process Characteristics

| Name                                     | Unit                                | Option |
|--|-------------------------------------|--------|
| SOLIDS RECOVERY RATIO                    |                                     | M1 (1) |
| SUSPENDED SOLIDS CONCENTRATION OF SLUDGE | (KG/M <sup>3</sup> )                | M2 (2) |
| DESIGN OVERFLOW RATE                     | (M <sup>3</sup> /M <sup>2</sup> *H) | M3 (3) |
| DESIGN SOLIDS LOADING RATE               | (KG/M <sup>2</sup> *D)              | M4 (4) |

### Specification Example



=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 6 }  
PROCESS NAME : THICK }

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y }

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 8 }  
SECOND INPUT STREAM NUMBER (IS2) : 0 }  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 9 }  
SECOND OUTPUT STREAM NUMBER (OS2) : 10 }

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y }

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: THICK

|  |  |                 |
|--|--|-----------------|
| SOLIDS RECOVERY RATIO                            |  | : <u>0.95</u> } |
| SUSPENDED SOLIDS CONCENTRATION OF SLUDGE (KG/M3) |  | : <u>50.</u> }  |
| DESIGN OVERFLOW RATE (M3/M2*H)                   |  | : <u>0.75</u> } |
| DESIGN SOLIDS LOADING RATE (KG/M3*DAY)           |  | : <u>50.</u> }  |

=====  
E N D C H A R A C T E R I S T I C S

## Process Model

### A. ASSUMPTIONS

1. No changes in the concentrations of dissolved matter.
2. Particulate matter concentrations in the output streams are proportional to the suspended solids concentrations.
3. Different specific gravity in the output streams are not accounted for.

### B. MODEL PRINCIPLES

1. Dissolved matter concentrations: Output=Input
2. Particulate matter:
  - a) A mass balance on suspended solids, giving the flow rates for the water effluent and the sludge stream.
  - b) The concentrations of the constituents connected to suspended solids are calculated from mass balances, in which the principle of homogeneous mixing are applied.
3. Special parameters for sludge quality in the output sludge stream are set equal to the input values.



#### 4. SYSTEM DESCRIPTION

The system is designed to be flexible and easy to update and change. This goal is reached by using a hierarchical module configuration. The main system level consists of the modules in Fig. 4.1.

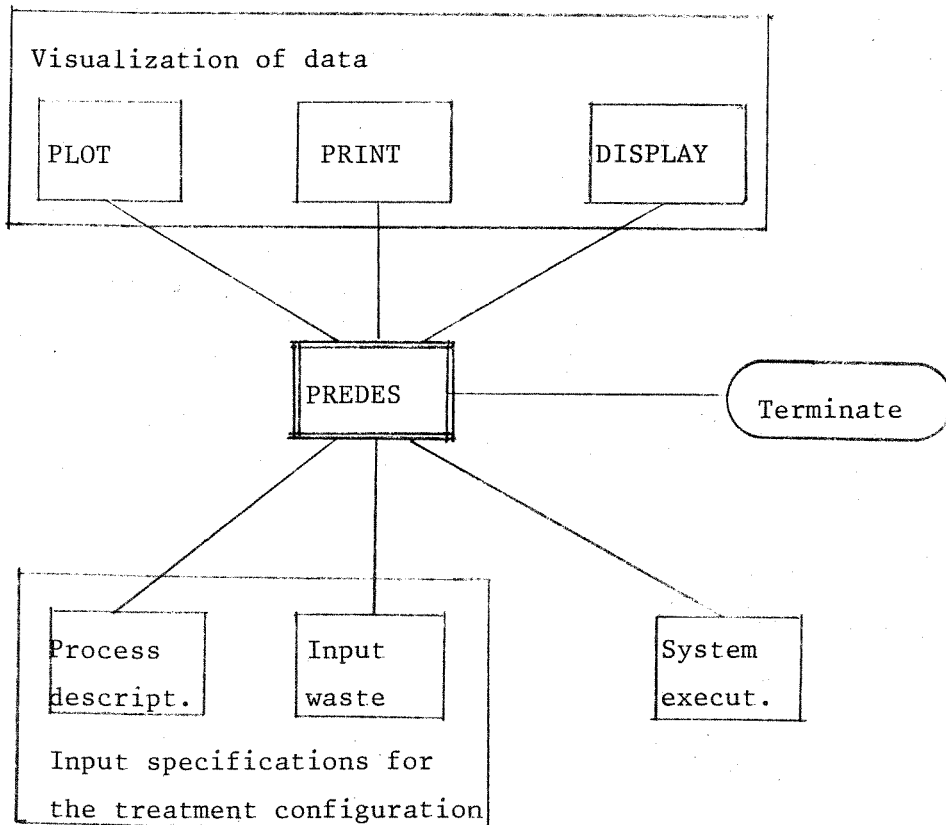


Fig. 4.1. Main modules

When starting the system by typing APREDES, you have to specify a file where to store/retrieve data. If you create a new file, you also have to specify design flows by Qdim and Qmaxdim. Then you can choose which module to execute by typing a digit corresponding to this module.

The choices look like this:

CHOOSE ONE OF THE FOLLOWING OPERATIONS:

- 3. PLOT
- 2. PRINT
- 1. DISPLAY
- 0. TERMINATE
- 1. PROCESS SPECIFICATION
- 2. WASTEWATER SPECIFICATION
- 3. ITERATE

:X<sub>2</sub>

Let us look into each of the main modules and see how they function.

#### 4.1 Plot

This module is not implemented yet.

#### 4.2 Print

This module gives a printed documentation of the input values and the results.

The PRINT module is splitted into five other modules, shown in Fig. 4.2. The system has one module for each kind of table to be printed out.

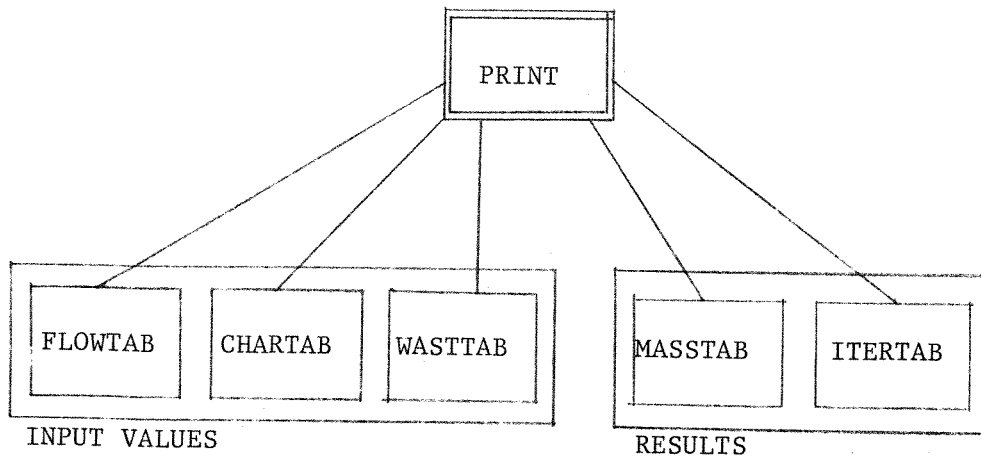


Fig. 4.2 Print modules

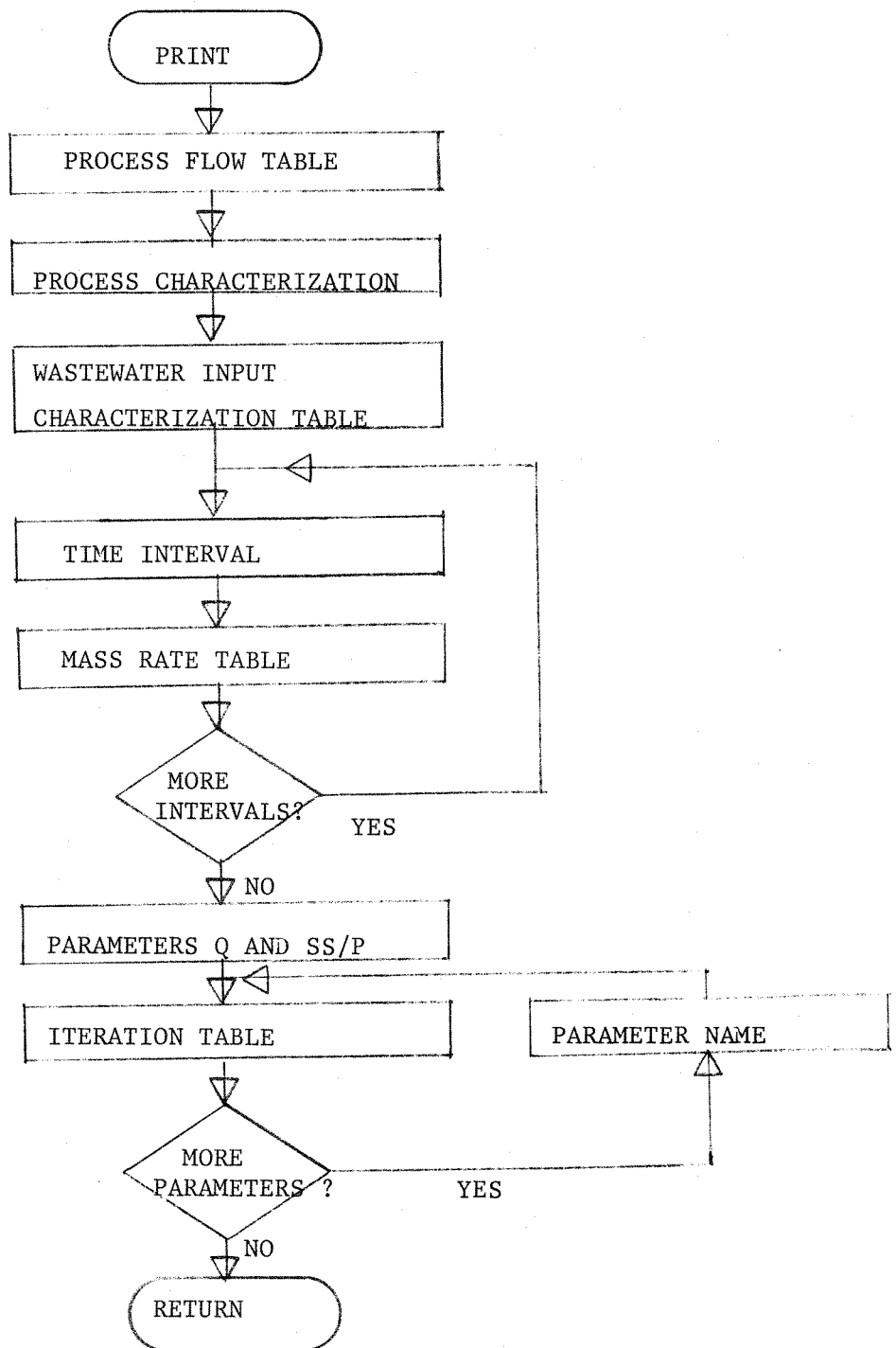
Entering the PRINT module, you automatically get printouts of the tables concerning the input values.

The tables are:

- Process flow table
- Process characterization table
- Wastewater input characterization table

Concerning the result tables, you have a flexibility. For instance, you can choose time interval (hour, day or year) for the Mass Rate Table, and if you like, you can set tables for all the intervals.

For the iteration table, you automatically get printouts of the tables for the parameters Q and SS/P. If you like, you can choose other /all parameters for the iteration table.



We will give a description of each table.

Process flow table (FLOWTAB)

This table shows which processes the treatment plant consists of, and how the processes are linked together. The tables also contain the design flows by Qdim and Qmaxdim.

QDIM :  
QMAXDIM :

| Identification |              | Flow |     |     |     |
|----------------|--------------|------|-----|-----|-----|
| N              | Process name | IS1  | IS2 | OS1 | OS2 |
|                |              |      |     |     |     |

Process characterization table (CHARTAB)

This table shows each process and its corresponding characterization. The process is identified by number and name, and its characterization by a number. The number is explained in section 3 under the corresponding process.

| Identification |              | Characterization |   |  |    |
|----------------|--------------|------------------|---|--|----|
| N              | Process name | 1                | 2 |  | 20 |
|                |              |                  |   |  |    |

Wastewater input characterization table (WASTTAB)

This table shows the specified values for each parameter. The different parameters are described in section 3.

Stream no.: X

| Parameter | Unit | Value |
|-----------|------|-------|
|           |      |       |

Mass rate table (MASSTAB)

This table shows the mass rates for each parameter and stream. The mass rates are calculated by multiplication of the final iterated stream flows, concentrations and specified time interval.

Time interval: X

| Stream number                        | Parameters |     |      |  |    |
|--------------------------------------|------------|-----|------|--|----|
|                                      | SS         | VSS | BaF7 |  | MG |
| X Particulated<br>Dissolved<br>Total |            |     |      |  |    |

Iteration table (ITERTAB)

This table shows the parameter values for the three first and the four last iterations for each stream. It also gives the relative differences between the last two iterations.

### 4.3 Display

By this module you have the opportunity to display data on the terminal, for visualization and control of input data and/or results.

The module is splitted into five other modules, one module for each table to be displayed, see Fig. 4.3.

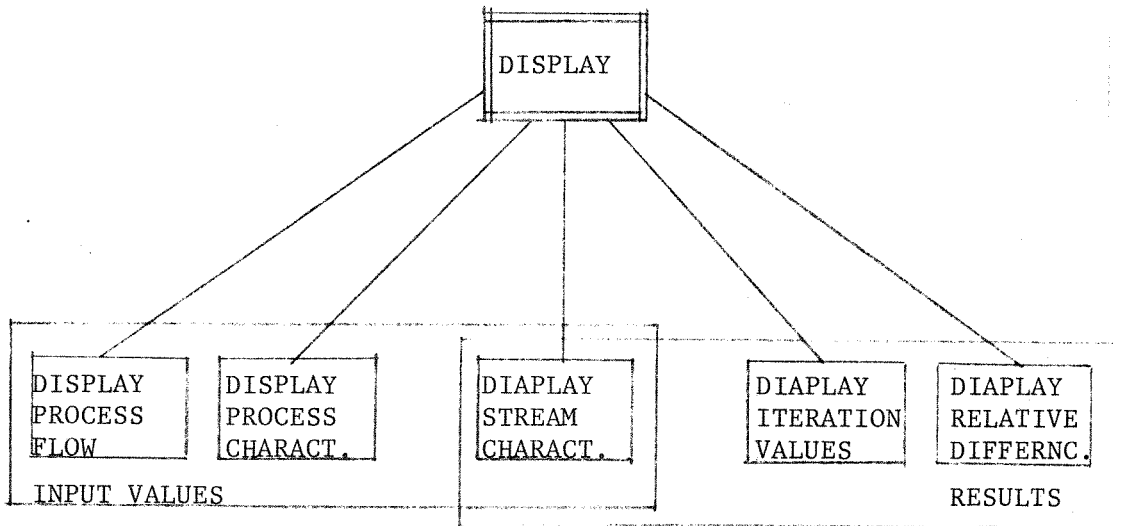


Fig. 4.3 DISPLAY module

Before starting the iterations, you should control the input data. Enterring the DISPLAY module, you can choose which table(s) to display by typing a digit corresponding to the actual table.

The choises are:

CHOOSE ONE OF THE FOLLOWING DISPLAY MODES:

0. RETURN FROM DISPLAY MODE
1. PROCESS FLOW
2. PROCESS CHARACTERISTICS
3. STREAM CHARACTERISTICS
4. ITERATION VALUES
5. RELATIVE DIFFERENCES

: X<sub>2</sub>





Display stream characterization (DISPSTCH)

Not implemented yet.

Display iteration values (DISPITER)

Not implemented yet.

Display relative differences (DISPDIFF)

This module permits you to display the relative differences for all the actual streams and specified parameters.

#### 4.4 Process description

This module is entered when you specify processes. The PROCESS DESCRIPTION module consists of three other modules, Fig. 4.4.

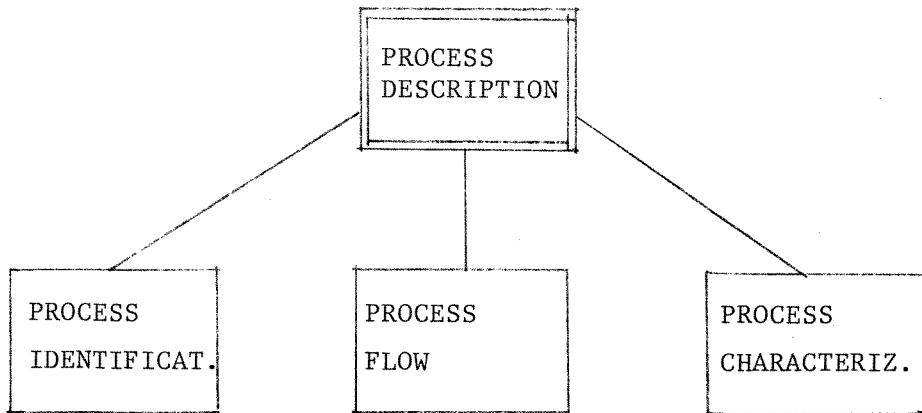


Fig. 4.4 PROCESS DESCRIPTION module

The PROCESS IDENTIFICATION module is used to specify the processes in the plant and to relate the process number to a process name. The legal process names are given in section 3.

PROCESS NUMBER : X ✓  
PROCESS NAME : X ✓

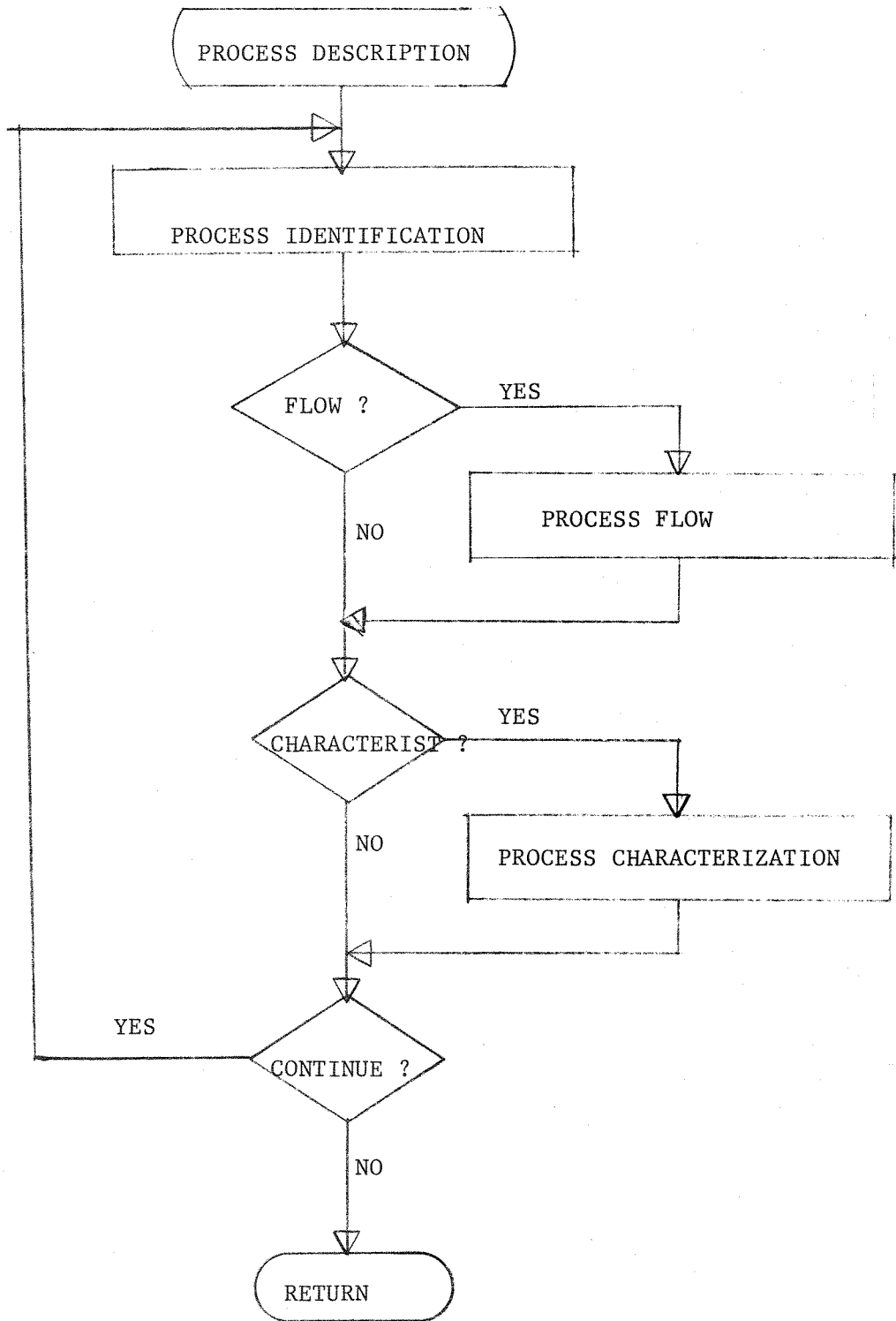
The PROCESS FLOW module is used to assign numbers to the input and output process streams. Zero value for a stream number indicate no stream.

After identification:

PRINCIPAL INPUT STREAM NUMBER (IS1): X ✓  
SECOND INPUT STREAM NUMBER (IS2): X ✓  
PRINCIPAL OUTPUT STREAM NUMBER(OS1): X ✓  
SECOND OUTPUT STREAM NUMBER(OS2): X ✓

The PROCESS CHARACTERIZATION module is used to describe the characteristics of a given process. The characteristics for all implemented processes are described in section 3.

When you enter the PROCESS DESCRIPTION module, the following chart shows what happens:



#### 4.5 Input wastewater characterization

This module is used to specify the input parameter values for a waste stream. The parameters are described in section 2.

If you specify a zero value for the flow rate, the earlier waste characterization of the given stream will be deleted.

#### 4.6 Iteration

This is a time consuming module, so you should check the input values before starting the iterations.

For the given design flows, process descriptions and input waste characterizations, the process models are run in at least seven iterations. You can specify the number of iterations you want to run (default value is 7). You can also specify the execution sequence of the processes. The execution sequence will otherwise be of raising order.

If a steady-state situation is not reached after the specified number of iterations, you can go on with more iterations until you are pleased.

The process models are all of the steady-state type.

## 5. COMPLETE EXAMPLE

In this section a practical application of the system is described.

We want to realize the following treatment plant:

1) Plant configuration as shown in Fig. 5.1

2) Design flows:

$Q_{dim} = 70. \text{ m}^3/\text{h}$   
 $Q_{maxdim} = 100. \text{ m}^3/\text{h}$

3) Input wastewater stream no.1 with the following specifications:

| Q    | 70. m <sup>3</sup> /h |             |                         |
|------|-----------------------|-------------|-------------------------|
|      |                       | Particulate | Dissolved               |
| SS   | 0.2                   |             | kg/m <sup>3</sup>       |
| VSS  | 0.15                  |             | kg/m <sup>3</sup>       |
| BOF7 | 0.15                  |             | 0.10 kg/m <sup>3</sup>  |
| P    | 0.003                 |             | 0.006 kg/m <sup>3</sup> |
| N    | 0.003                 |             | 0.014 kg/m <sup>3</sup> |
| CD   | 0.005                 |             | 0.005 g/m <sup>3</sup>  |
| HG   | 0.005                 |             | 0.005 g/m <sup>3</sup>  |
| FB   | 0.003                 |             | 0.003 g/m <sup>3</sup>  |
| CA   | 0.0005                |             | 0.020 kg/m <sup>3</sup> |
| MG   | 0.0005                |             | 0.005 kg/m <sup>3</sup> |
| ALK  |                       |             | 2.8 eq/m <sup>3</sup>   |
| PH   |                       |             | 7.2                     |

### Special parameters

|         |     |
|---------|-----|
| HYGIENE | 10. |
| ODOR    | 10. |
| PPROT   | 10. |

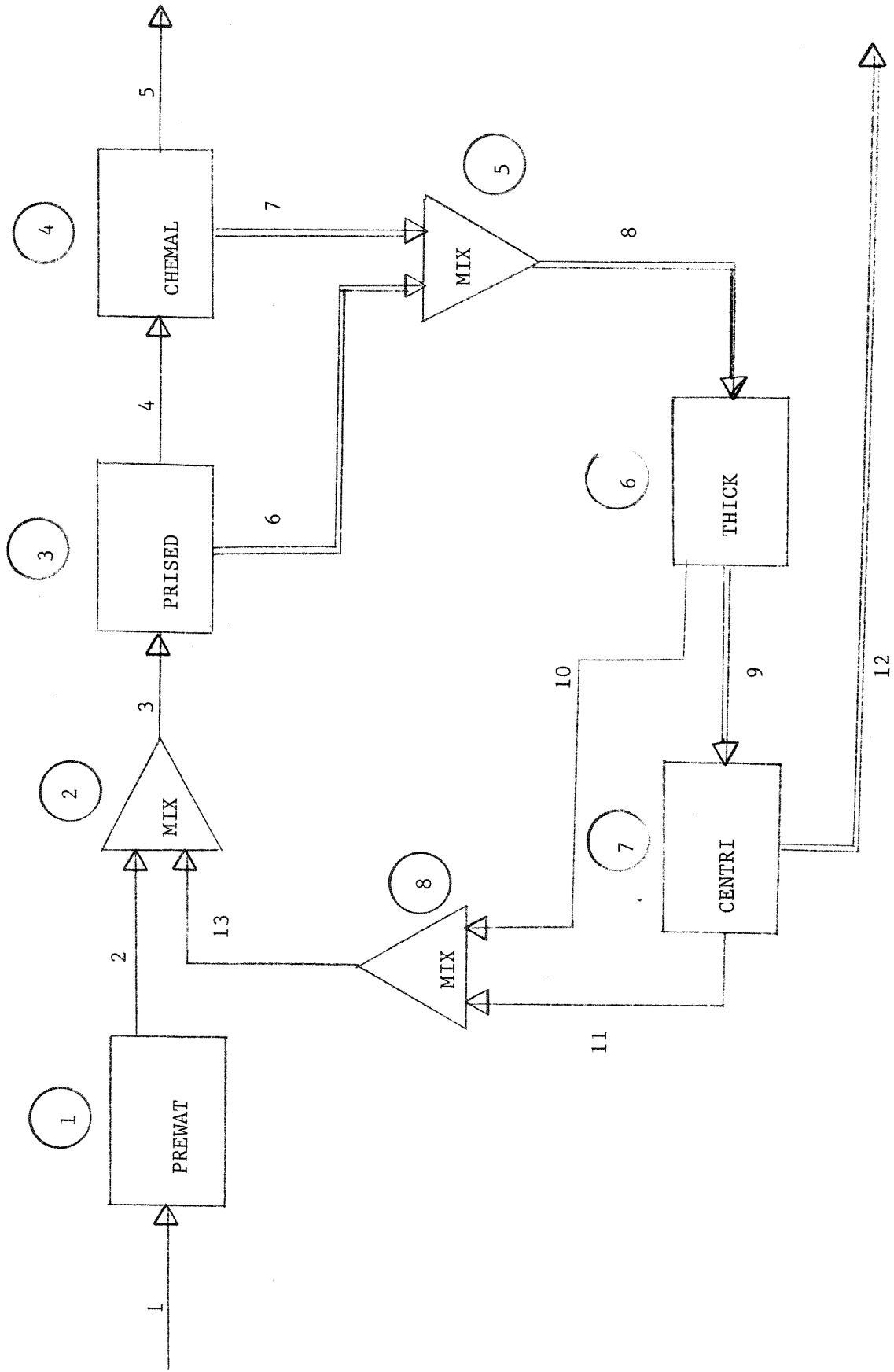
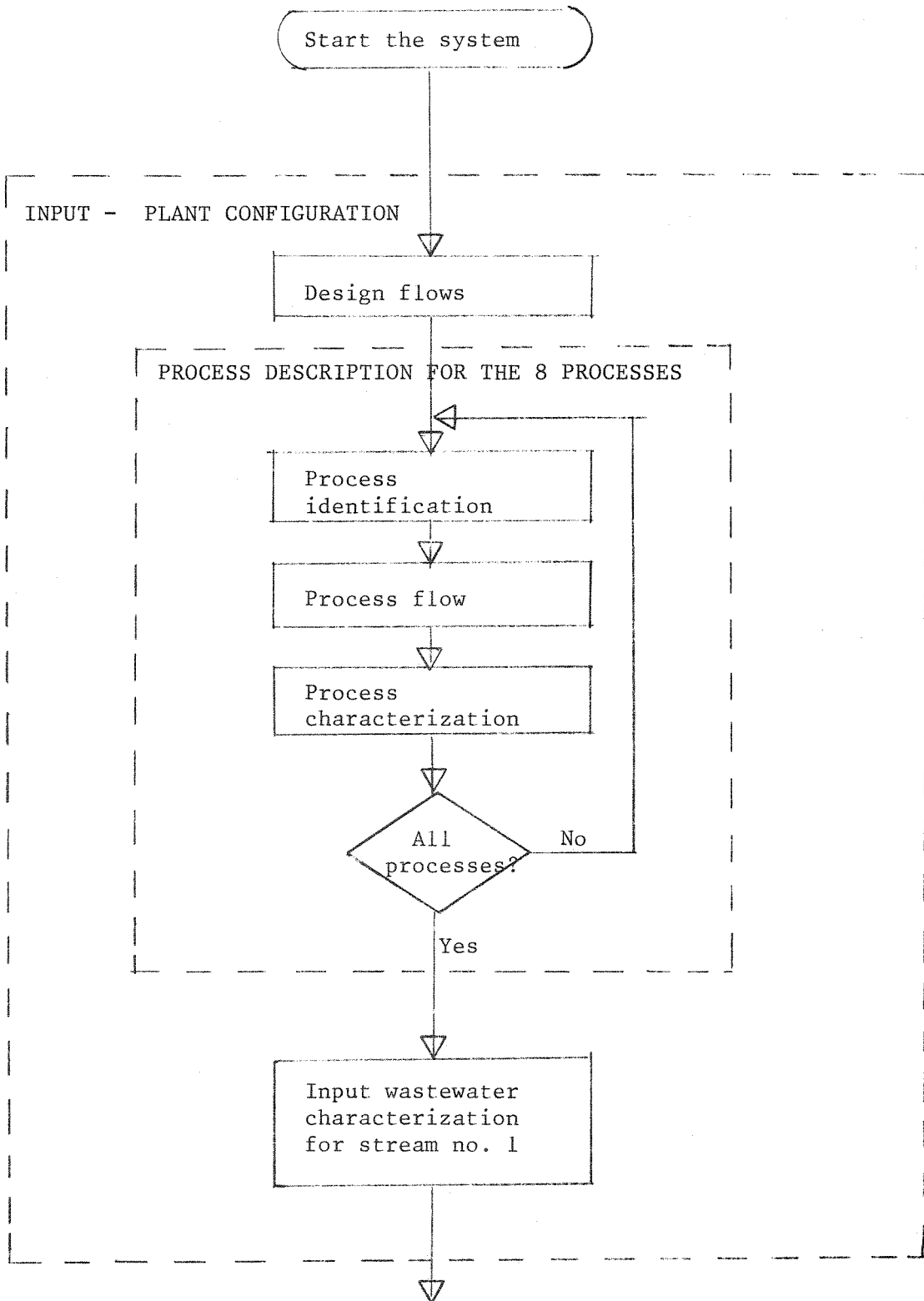
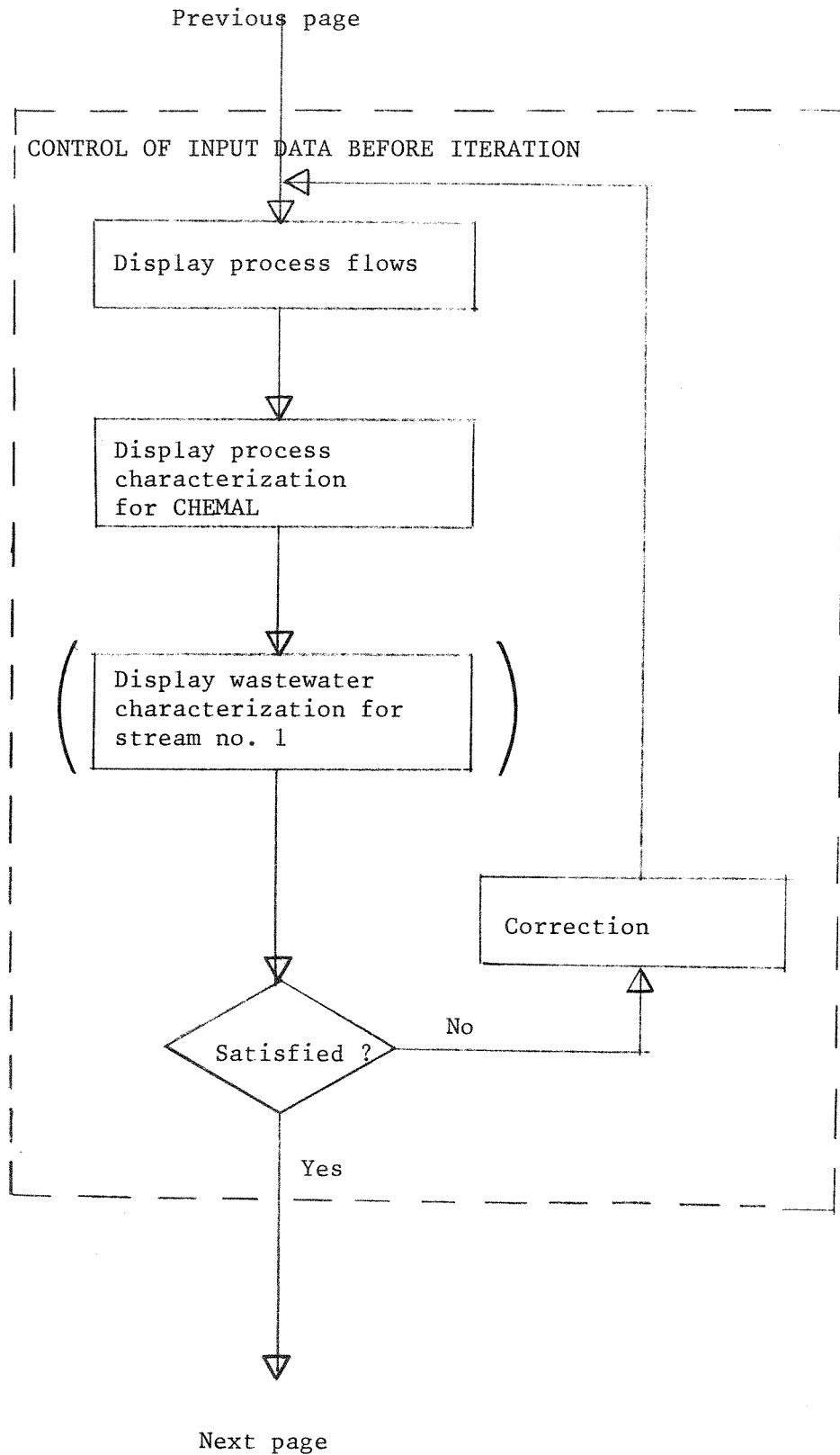


Fig. 5.1. Wastewater treatment plant configuration.

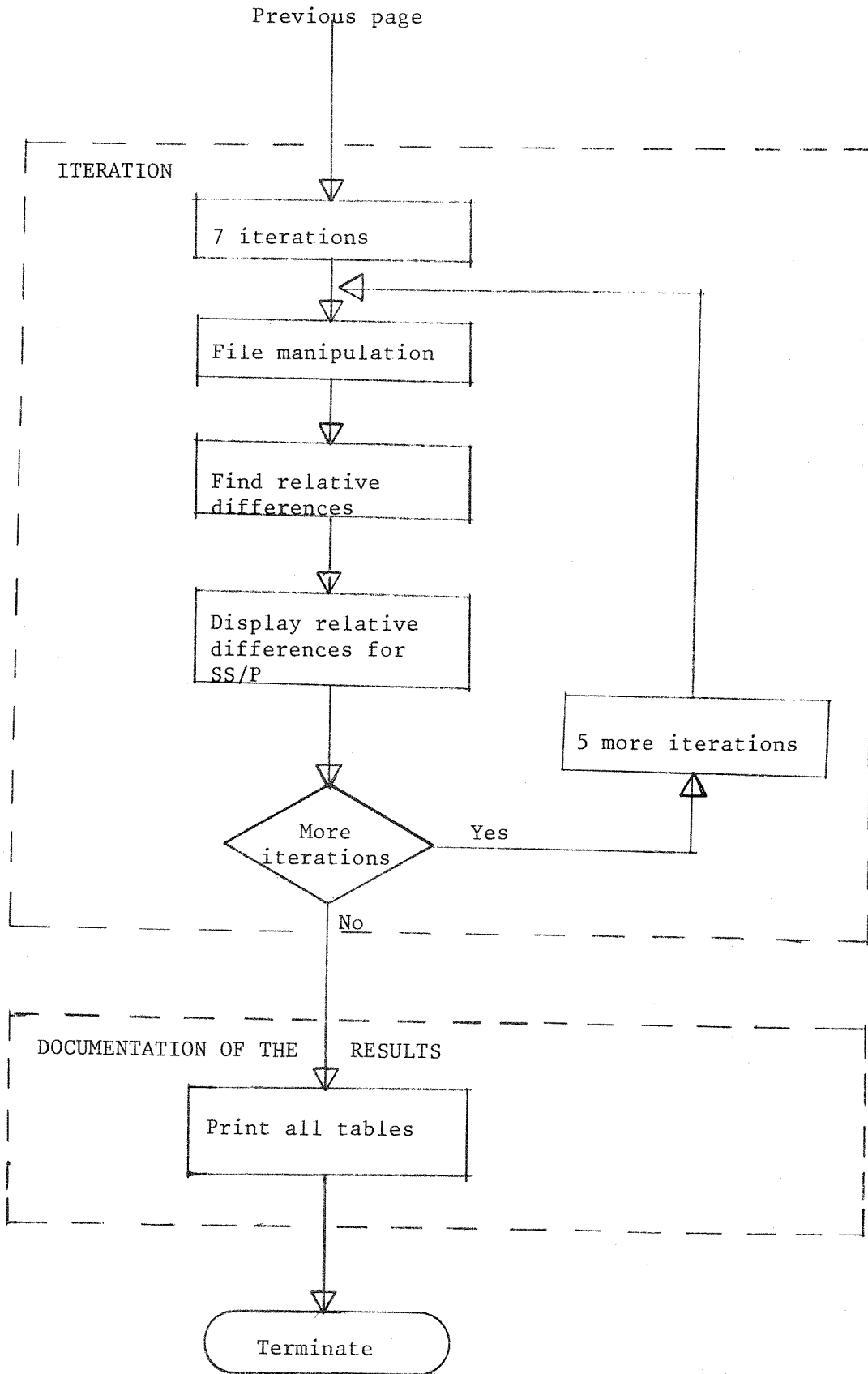
Before we enter PREDES, let us outline what we are going to do.



Next page









===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 1 ↘  
PROCESS NAME : PREWAT ↘

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ↘

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 1 ↘  
SECOND INPUT STREAM NUMBER (IS2) : 0 ↘  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 2 ↘  
SECOND OUTPUT STREAM NUMBER (OS2) : 0 ↘

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ↘

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: PREWAT

===== E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y ↘

=====  
P R O C E S S I D E N T I F I C A T I O NPROCESS NUMBER (N) : 2  
PROCESS NAME : MIX=====  
E N D I D E N T I F I C A T I O N? DO YOU WANT TO SPECIFY PROCESS FLOW? Y=====  
P R O C E S S F L O WPRINCIPAL INPUT STREAM NUMBER (IS1) : 2  
SECOND INPUT STREAM NUMBER (IS2) : 13  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 3  
SECOND OUTPUT STREAM NUMBER (OS2) : 0=====  
E N D F L O W? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: MIX

=====  
E N D C H A R A C T E R I S T I C S? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y

=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 3  
PROCESS NAME : PRISED

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 3  
SECOND INPUT STREAM NUMBER (IS2) : 0  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 4  
SECOND OUTPUT STREAM NUMBER (OS2) : 5

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: PRISED

\* SEDIMENTATION BASIN

OVERFLOW RATE AT QDIM (M3/M2/H) : 1.9  
AT QMAXDIM (M3/M2/H) : 3.8  
DETENTION TIME AT QDIM (H) :     
DEPTH (M) : 2.5

SUSPENDED SOLIDS CONCENTRATIONS:

WATER EFFLUENT (WHEN PREFIXED) (KG/M3) : 0.070  
PRIMARY SLUDGE (KG/M3) : 30.0

=====  
E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y

===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 4 ↘  
 PROCESS NAME : CHEMAL ↘

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ↘

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 4 ↘  
 SECOND INPUT STREAM NUMBER (IS2) : 0 ↘  
 PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 5 ↘  
 SECOND OUTPUT STREAM NUMBER (OS2) : 7 ↘

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ↘

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: CHEMAL

\* CHEMICAL ADDITION  
 PRECIPITATION PH : 5.9 ↘

\* FLOCCULATION  
 TEMPERATURE (DEG C) : 10. ↘  
 NUMBER OF CHAMBERS : 3. ↘  
 TOTAL DETENTION TIME AT QDIM (MIN) : 30. ↘

\* SEDIMENTATION BASIN  
 OVERFLOW RATE AT QDIM (M3/M2/H) : 1.3 ↘  
 AT QMAXDIM (M3/M2/H) : 2.0 ↘  
 DETENTION TIME AT QDIM (H) : 2 ↘  
 DEPTH (M) : 2.5 ↘

SUSPENDED SOLIDS CONCENTRATIONS:  
 WATER EFFLUENT (WHEN PREFIXED) (KG/M3) : 0.015 ↘  
 CHEMICAL SLUDGE (KG/M3) : 7.5 ↘

===== E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y ↘

===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 5 ↘  
PROCESS NAME : MIX ↘

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y ↘

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 7 ↘  
SECOND INPUT STREAM NUMBER (IS2) : 6 ↘  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 8 ↘  
SECOND OUTPUT STREAM NUMBER (OS2) : 0 ↘

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y ↘

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: MIX

===== E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y ↘

=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 6 }  
PROCESS NAME : THICK }

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y }

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 8 }  
SECOND INPUT STREAM NUMBER (IS2) : 0 }  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 9 }  
SECOND OUTPUT STREAM NUMBER (OS2) : 10 }

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y }

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: THICK

SOLIDS RECOVERY RATIO : 0.95 }  
SUSPENDED SOLIDS CONCENTRATION OF SLUDGE (KG/M3) : 50. }  
DESIGN OVERFLOW RATE (M3/M2\*H) : 0.75 }  
DESIGN SOLIDS LOADING RATE (KG/M3\*DAY) : 50. }

=====  
E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y }



=====  
P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 2  
PROCESS NAME : CENTRI

=====  
E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

=====  
P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 9  
SECOND INPUT STREAM NUMBER (IS2) : 0  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 12  
SECOND OUTPUT STREAM NUMBER (OS2) : 11

=====  
E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

=====  
P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: CENTRI

SOLIDS RECOVERY RATIO FOR CENTRIFUGATION : 0.95  
SUSPENDED SOLIDS CONCENTRATION OF SLUDGE : 200.  
OUTPUT STREAM (KG/M3)

=====  
E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? Y

===== P R O C E S S I D E N T I F I C A T I O N

PROCESS NUMBER (N) : 8  
PROCESS NAME : MIX

===== E N D I D E N T I F I C A T I O N

? DO YOU WANT TO SPECIFY PROCESS FLOW? Y

===== P R O C E S S F L O W

PRINCIPAL INPUT STREAM NUMBER (IS1) : 10  
SECOND INPUT STREAM NUMBER (IS2) : 11  
PRINCIPAL OUTPUT STREAM NUMBER (OS1) : 13  
SECOND OUTPUT STREAM NUMBER (OS2) : 0

===== E N D F L O W

? DO YOU WANT TO GIVE PROCESS CHARACTERISTICS? Y

===== P R O C E S S C H A R A C T E R I S T I C S

PROCESS NAME: MIX

===== E N D C H A R A C T E R I S T I C S

? DO YOU WANT TO CONTINUE WITH PROCESS SPECIFICATIONS? N

CHOOSE ONE OF THE FOLLOWING OPERATIONS:

- 3. PLOT
- 2. PRINT
- 1. DISPLAY
  
- 0. TERMINATE
  
- 1. PROCESS SPECIFICATION
- 2. WASTEWATER SPECIFICATION
  
- 3. ITERATE

2

===== W A S T E W A T E R CHARACTERIZATION

INPUT STREAM NUMBER: 1

FLOW RATE (Q) (M3/H) : 70.

\* PARTICULATE MATTER:

|        |         |                 |
|--------|---------|-----------------|
| SS/P   | (KG/M3) | : <u>0.200</u>  |
| VSS/P  | (KG/M3) | : <u>0.150</u>  |
| BOF7/P | (KG/M3) | : <u>0.150</u>  |
| P/P    | (KG/M3) | : <u>0.003</u>  |
| N/P    | (KG/M3) | : <u>0.003</u>  |
| CD/P   | (G/M3)  | : <u>0.005</u>  |
| HG/P   | (G/M3)  | : <u>0.005</u>  |
| PB/P   | (G/M3)  | : <u>0.003</u>  |
| CA/P   | (KG/M3) | : <u>0.0005</u> |
| MG/P   | (KG/M3) | : <u>0.0005</u> |

\* DISSOLVED MATTER:

|        |         |                |
|--------|---------|----------------|
| BOF7/D | (KG/M3) | : <u>0.100</u> |
| P/D    | (KG/M3) | : <u>0.006</u> |
| N/D    | (KG/M3) | : <u>0.014</u> |
| CD/D   | (G/M3)  | : <u>0.005</u> |
| HG/D   | (G/M3)  | : <u>0.005</u> |
| PB/D   | (G/M3)  | : <u>0.003</u> |
| CA/D   | (KG/M3) | : <u>0.020</u> |
| MG/D   | (KG/M3) | : <u>0.005</u> |
| ALK/D  | (MEKV.) | : <u>2.8</u>   |
| PH/D   |         | : <u>7.2</u>   |

\* SPECIAL PARAMETERS:

|           |        |              |
|-----------|--------|--------------|
| HYGIENE/S | (0-10) | : <u>10.</u> |
| ODOR/S    | (0-10) | : <u>10.</u> |
| PPROT/S   | (0-10) | : <u>10.</u> |

? DO YOU WANT TO CONTINUE WITH CHARACTERIZATION? N

===== E N D CHARACTERIZATION



CHOOSE ONE OF THE FOLLOWING DISPLAY MODES:

- 0. RETURN FROM DISPLAY MODE
- 1. PROCESS FLOW
- 2. PROCESS CHARACTERISTICS
- 3. STREAM CHARACTERISTICS
- 4. ITERATION VALUES
- 5. RELATIVE DIFFERENCES

2 →

PROCESS NUMBER: 4 →

PROCESS CHARACTERIZATION

| PROCESS NUMBER: 4 | CHEMAL | CHAR. NUMBER : | VALUE  |
|-------------------|--------|----------------|--------|
|                   |        | 1              | 5.900  |
|                   |        | 2              |        |
|                   |        | 3              |        |
|                   |        | 4              | 10.000 |
|                   |        | 5              | 3.000  |
|                   |        | 6              | 30.000 |
|                   |        | 7              | 1.300  |
|                   |        | 8              | 2.000  |
|                   |        | 9              | 0.054  |
|                   |        | 10             | 1.923  |
|                   |        | 11             | -2.500 |
|                   |        | 12             | 0.135  |
|                   |        | 13             | 0.015  |
|                   |        | 14             | 7.500  |
|                   |        | 15             |        |
|                   |        | 16             |        |
|                   |        | 17             |        |
|                   |        | 18             |        |
|                   |        | 19             |        |
|                   |        | 20             |        |

?

ARE YOU SATISFIED WITH THE CHARACTERISTIC? Y →

?

DO YOU WANT TO DISPLAY MORE PROCESS CHARACTERISTICS? N →

CHOOSE ONE OF THE FOLLOWING DISPLAY MODES:

- 0. RETURN FROM DISPLAY MODE
- 1. PROCESS FLOW
- 2. PROCESS CHARACTERISTICS
- 3. STREAM CHARACTERISTICS
- 4. ITERATION VALUES
- 5. RELATIVE DIFFERENCES

0 →

===== E N D DISPLAY MODE

CHOOSE ONE OF THE FOLLOWING OPERATIONS:

- 3. PLOT
- 3. PRINT
- 1. DISPLAY
  
- 0. TERMINATE
  
- 1. PROCESS SPECIFICATION
- 2. WASTEWATER SPECIFICATION
  
- 3. ITERATE

3 →

?

DO YOU WANT TO SPECIFY NUMBER OF ITERATIONS (DEFAULT 7)? →

?

DO YOU WANT TO SPECIFY THE ITERATION SEQUENCE? →

ITERATION - WAIT!

```

ITERATION NUMBER: 1
ITERATION NUMBER: 2
  PROCESS EXECUTED: 1
  PROCESS EXECUTED: 2
  PROCESS EXECUTED: 3
  PROCESS EXECUTED: 4
  PROCESS EXECUTED: 5
  PROCESS EXECUTED: 6
  PROCESS EXECUTED: 7
  PROCESS EXECUTED: 8
ITERATION NUMBER: 3
  PROCESS EXECUTED: 1
  PROCESS EXECUTED: 2
  PROCESS EXECUTED: 3
  PROCESS EXECUTED: 4
  PROCESS EXECUTED: 5
  PROCESS EXECUTED: 6
  PROCESS EXECUTED: 7
  PROCESS EXECUTED: 8
ITERATION NUMBER: 4
  PROCESS EXECUTED: 1
  PROCESS EXECUTED: 2
  PROCESS EXECUTED: 3
  PROCESS EXECUTED: 4
  PROCESS EXECUTED: 5
  PROCESS EXECUTED: 6
  PROCESS EXECUTED: 7
  PROCESS EXECUTED: 8
ITERATION NUMBER: 5
  PROCESS EXECUTED: 1
  PROCESS EXECUTED: 2
  PROCESS EXECUTED: 3
  PROCESS EXECUTED: 4
  PROCESS EXECUTED: 5
  PROCESS EXECUTED: 6
  PROCESS EXECUTED: 7
  PROCESS EXECUTED: 8
ITERATION NUMBER: 6
  PROCESS EXECUTED: 1
  PROCESS EXECUTED: 2
  PROCESS EXECUTED: 3
  PROCESS EXECUTED: 4
  PROCESS EXECUTED: 5
  PROCESS EXECUTED: 6
  PROCESS EXECUTED: 7
  PROCESS EXECUTED: 8

```

ITERATION NUMBER: 7  
PROCESS EXECUTED: 1  
PROCESS EXECUTED: 2  
PROCESS EXECUTED: 3  
PROCESS EXECUTED: 4  
PROCESS EXECUTED: 5  
PROCESS EXECUTED: 6  
PROCESS EXECUTED: 7  
PROCESS EXECUTED: 8

FILE MANIPULATIONS - WAIT!

FIND RELATIVE DIFFERENCES - WAIT!

RELATIVE DIFFERENCE(%) FOR PARAMETER: SS/P

|             |    |      |             |    |      |
|-------------|----|------|-------------|----|------|
| STREAM NO.: | 1  | 0.00 | STREAM NO.: | 2  | 0.00 |
| STREAM NO.: | 3  | 0.00 | STREAM NO.: | 4  | 0.00 |
| STREAM NO.: | 5  | 0.00 | STREAM NO.: | 6  | 0.00 |
| STREAM NO.: | 7  | 0.00 | STREAM NO.: | 8  | 0.00 |
| STREAM NO.: | 9  | 0.00 | STREAM NO.: | 10 | 0.00 |
| STREAM NO.: | 11 | 0.00 | STREAM NO.: | 12 | 0.00 |
| STREAM NO.: | 13 | 0.00 |             |    |      |

?

DO YOU WANT TO CONTINUE WITH 5 MORE ITERATIONS? N →

CHOOSE ONE OF THE FOLLOWING OPERATIONS:

- 3. PLOT
- 2. PRINT
- 1. DISPLAY
  
- 0. TERMINATE
  
- 1. PROCESS SPECIFICATION
- 2. WASTEWATER SPECIFICATION
  
- 3. ITERATE

-2 →

PRINT ON LF- WAIT!

PROCESS FLOW TABLE  
PROCESS CHARACTERIZATION TABLE  
WASTEWATER TABLE  
MASS RATE TABLE

CHOOSE TIME INTERVAL

- 1. HOUR
- 2. DAY
- 3. YEAR

1 →

?

DO YOU WANT TO GIVE A NEW TIME INTERVAL? Y →

CHOOSE TIME INTERVAL

- 1. HOUR
- 2. DAY
- 3. YEAR

2 →

?

DO YOU WANT TO GIVE A NEW TIME INTERVAL? Y →

CHOOSE TIME INTERVAL

- 1. HOUR
- 2. DAY
- 3. YEAR

3 →

?

DO YOU WANT TO GIVE A NEW TIME INTERVAL? N →



ITERATION TABLE

Q

SS/F

?

DO YOU WANT TO PRINT ITERATION-TABLE FOR MORE PARAMETERS? Y →

PARAMETER NAME: ALL →

USS/F

BOF7/F

F/F

N/F

CD/F

HG/F

FB/F

CA/F

MG/F

BOF7/D

F/D

N/D

CD/D

HG/D

FB/D

CA/D

MG/D

ALK/D

PH/D

HYGIENE/S

ODOR/S

PFROT/S

?

DO YOU WANT TO PRINT ITERATION-TABLE FOR MORE PARAMETERS? N →







PROCESS CHARACTERIZATION TABLE

| IDENTIFICATION |              | CHARACTERIZATION |         |       |        |       |        |       |        |       |       |
|----------------|--------------|------------------|---------|-------|--------|-------|--------|-------|--------|-------|-------|
| 1              | PROCESS NAME | 1                | 2       | 3     | 4      | 5     | 6      | 7     | 8      | 9     | 10    |
| 1              | PREMAT       | 0.000            | 0.000   | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000 |
| 2              | MIX          | 0.000            | 0.000   | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000 |
| 3              | PRISED       | 1.900            | 3.800   | 0.037 | 1.316  | 2.500 | 0.092  | 0.070 | 30.000 | 0.000 | 0.000 |
| 4              | CHEMAL       | 5.900            | 259.332 | 3.402 | 10.000 | 3.000 | 30.000 | 1.300 | 2.000  | 0.054 | 1.023 |
| 5              | MIX          | 0.000            | 0.000   | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000 |
| 6              | THICK        | 0.950            | 50.000  | 0.750 | 50.000 | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000 |
| 7              | CHTRI        | 0.950            | 200.000 | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000 |
| 8              | MIX          | 0.000            | 0.000   | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000  | 0.000 | 0.000 |
| 9              |              |                  |         |       |        |       |        |       |        |       |       |
| 10             |              |                  |         |       |        |       |        |       |        |       |       |
| 11             |              |                  |         |       |        |       |        |       |        |       |       |
| 12             |              |                  |         |       |        |       |        |       |        |       |       |
| 13             |              |                  |         |       |        |       |        |       |        |       |       |
| 14             |              |                  |         |       |        |       |        |       |        |       |       |
| 15             |              |                  |         |       |        |       |        |       |        |       |       |
| 16             |              |                  |         |       |        |       |        |       |        |       |       |
| 17             |              |                  |         |       |        |       |        |       |        |       |       |
| 18             |              |                  |         |       |        |       |        |       |        |       |       |
| 19             |              |                  |         |       |        |       |        |       |        |       |       |
| 20             |              |                  |         |       |        |       |        |       |        |       |       |
| 21             |              |                  |         |       |        |       |        |       |        |       |       |
| 22             |              |                  |         |       |        |       |        |       |        |       |       |
| 23             |              |                  |         |       |        |       |        |       |        |       |       |
| 24             |              |                  |         |       |        |       |        |       |        |       |       |
| 25             |              |                  |         |       |        |       |        |       |        |       |       |
| 26             |              |                  |         |       |        |       |        |       |        |       |       |
| 27             |              |                  |         |       |        |       |        |       |        |       |       |
| 28             |              |                  |         |       |        |       |        |       |        |       |       |
| 29             |              |                  |         |       |        |       |        |       |        |       |       |
| 30             |              |                  |         |       |        |       |        |       |        |       |       |
| 31             |              |                  |         |       |        |       |        |       |        |       |       |
| 32             |              |                  |         |       |        |       |        |       |        |       |       |
| 33             |              |                  |         |       |        |       |        |       |        |       |       |
| 34             |              |                  |         |       |        |       |        |       |        |       |       |
| 35             |              |                  |         |       |        |       |        |       |        |       |       |
| 36             |              |                  |         |       |        |       |        |       |        |       |       |
| 37             |              |                  |         |       |        |       |        |       |        |       |       |
| 38             |              |                  |         |       |        |       |        |       |        |       |       |
| 39             |              |                  |         |       |        |       |        |       |        |       |       |
| 40             |              |                  |         |       |        |       |        |       |        |       |       |
| 41             |              |                  |         |       |        |       |        |       |        |       |       |
| 42             |              |                  |         |       |        |       |        |       |        |       |       |
| 43             |              |                  |         |       |        |       |        |       |        |       |       |
| 44             |              |                  |         |       |        |       |        |       |        |       |       |
| 45             |              |                  |         |       |        |       |        |       |        |       |       |
| 46             |              |                  |         |       |        |       |        |       |        |       |       |
| 47             |              |                  |         |       |        |       |        |       |        |       |       |
| 48             |              |                  |         |       |        |       |        |       |        |       |       |
| 49             |              |                  |         |       |        |       |        |       |        |       |       |
| 50             |              |                  |         |       |        |       |        |       |        |       |       |
| 51             |              |                  |         |       |        |       |        |       |        |       |       |
| 52             |              |                  |         |       |        |       |        |       |        |       |       |
| 53             |              |                  |         |       |        |       |        |       |        |       |       |
| 54             |              |                  |         |       |        |       |        |       |        |       |       |
| 55             |              |                  |         |       |        |       |        |       |        |       |       |
| 56             |              |                  |         |       |        |       |        |       |        |       |       |
| 57             |              |                  |         |       |        |       |        |       |        |       |       |
| 58             |              |                  |         |       |        |       |        |       |        |       |       |
| 59             |              |                  |         |       |        |       |        |       |        |       |       |
| 60             |              |                  |         |       |        |       |        |       |        |       |       |
| 61             |              |                  |         |       |        |       |        |       |        |       |       |
| 62             |              |                  |         |       |        |       |        |       |        |       |       |
| 63             |              |                  |         |       |        |       |        |       |        |       |       |
| 64             |              |                  |         |       |        |       |        |       |        |       |       |
| 65             |              |                  |         |       |        |       |        |       |        |       |       |
| 66             |              |                  |         |       |        |       |        |       |        |       |       |
| 67             |              |                  |         |       |        |       |        |       |        |       |       |
| 68             |              |                  |         |       |        |       |        |       |        |       |       |
| 69             |              |                  |         |       |        |       |        |       |        |       |       |
| 70             |              |                  |         |       |        |       |        |       |        |       |       |
| 71             |              |                  |         |       |        |       |        |       |        |       |       |
| 72             |              |                  |         |       |        |       |        |       |        |       |       |
| 73             |              |                  |         |       |        |       |        |       |        |       |       |
| 74             |              |                  |         |       |        |       |        |       |        |       |       |
| 75             |              |                  |         |       |        |       |        |       |        |       |       |
| 76             |              |                  |         |       |        |       |        |       |        |       |       |
| 77             |              |                  |         |       |        |       |        |       |        |       |       |
| 78             |              |                  |         |       |        |       |        |       |        |       |       |
| 79             |              |                  |         |       |        |       |        |       |        |       |       |
| 80             |              |                  |         |       |        |       |        |       |        |       |       |
| 81             |              |                  |         |       |        |       |        |       |        |       |       |
| 82             |              |                  |         |       |        |       |        |       |        |       |       |
| 83             |              |                  |         |       |        |       |        |       |        |       |       |
| 84             |              |                  |         |       |        |       |        |       |        |       |       |
| 85             |              |                  |         |       |        |       |        |       |        |       |       |
| 86             |              |                  |         |       |        |       |        |       |        |       |       |
| 87             |              |                  |         |       |        |       |        |       |        |       |       |
| 88             |              |                  |         |       |        |       |        |       |        |       |       |
| 89             |              |                  |         |       |        |       |        |       |        |       |       |
| 90             |              |                  |         |       |        |       |        |       |        |       |       |
| 91             |              |                  |         |       |        |       |        |       |        |       |       |
| 92             |              |                  |         |       |        |       |        |       |        |       |       |
| 93             |              |                  |         |       |        |       |        |       |        |       |       |
| 94             |              |                  |         |       |        |       |        |       |        |       |       |
| 95             |              |                  |         |       |        |       |        |       |        |       |       |
| 96             |              |                  |         |       |        |       |        |       |        |       |       |
| 97             |              |                  |         |       |        |       |        |       |        |       |       |
| 98             |              |                  |         |       |        |       |        |       |        |       |       |
| 99             |              |                  |         |       |        |       |        |       |        |       |       |
| 100            |              |                  |         |       |        |       |        |       |        |       |       |

PROCESS CHARACTERIZATION TABLE

| IDENTIFICATION |              | CHARACTERIZATION |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
|----------------|--------------|------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4              | PROCESS NAME | 11               | 12    | 13    | 14    | 15    | 16    | 17    | 18    | 19    | 20    | 21    | 22    | 23    | 24    | 25    | 26    | 27    | 28    | 29    | 30    |       |
| 1              | PREPAT       | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 2              | MIX          | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 3              | PRESED       | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 4              | CHEMAT       | 2.500            | 0.135 | 0.015 | 7.500 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 5              | MIX          | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 6              | THICK        | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 7              | CENTRI       | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 8              | MIX          | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 9              |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 10             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 11             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 12             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 13             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 14             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 15             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 16             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 17             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 18             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 19             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 20             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 21             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 22             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 23             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 24             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 25             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 26             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 27             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 28             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 29             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |
| 30             |              |                  |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |

WASTEWATER INPUT CHARACTERIZATION TABLE

STREAM NUMBER: 1

| PARAMETER            | UNIT                 | VALUE     |
|----------------------|----------------------|-----------|
| Q                    | (M <sup>3</sup> /H)  | 70.000000 |
| * PARTICULATE MATTER |                      |           |
| SS/P                 | (KG/M <sup>3</sup> ) | 0.200000  |
| VSS/P                | (KG/M <sup>3</sup> ) | 0.150000  |
| HOPE7/P              | (KG/M <sup>3</sup> ) | 0.150000  |
| P/P                  | (KG/M <sup>3</sup> ) | 0.003000  |
| N/P                  | (KG/M <sup>3</sup> ) | 0.003000  |
| Cl/P                 | (G/M <sup>3</sup> )  | 0.005000  |
| HG/P                 | (G/M <sup>3</sup> )  | 0.005000  |
| PR/P                 | (G/M <sup>3</sup> )  | 0.003000  |
| CA/P                 | (KG/M <sup>3</sup> ) | 0.000500  |
| MG/P                 | (KG/M <sup>3</sup> ) | 0.000500  |
| * DISSOLVED MATTER   |                      |           |
| ROF7/D               | (KG/M <sup>3</sup> ) | 0.100000  |
| P/D                  | (KG/M <sup>3</sup> ) | 0.004000  |
| N/D                  | (KG/M <sup>3</sup> ) | 0.014000  |
| Cl/D                 | (G/M <sup>3</sup> )  | 0.005000  |
| HG/D                 | (G/M <sup>3</sup> )  | 0.005000  |
| PR/D                 | (G/M <sup>3</sup> )  | 0.003000  |
| CA/D                 | (KG/M <sup>3</sup> ) | 0.020000  |
| HG/D                 | (KG/M <sup>3</sup> ) | 0.005000  |
| ALK/D                | (MEKV.)              | 2.800000  |
| PH/D                 |                      | 7.200000  |
| * SPECIAL PARAMETERS |                      |           |
| HYGIENE/S            | (0-10)               | 10.000000 |
| ODOR/S               | (0-10)               | 10.000000 |
| PPROT/S              | (0-10)               | 10.000000 |

NVA - PIRPES

DATE: 1990-03-28

TIME: 09.15.12

PAGE: 4

MASS GATE TABLE

TIME INTERVAL: HOUR

PARAMETERS

| STREAM NUMBER | S <sub>1</sub> (KG/H) | VSS (KG/H) | BOF7 (KG/H) | P (KG/H) | N (KG/H) | CD (G/H) | HG (G/H) | PR (G/H) | CA (KG/H) | MG (KG/H) |
|---------------|-----------------------|------------|-------------|----------|----------|----------|----------|----------|-----------|-----------|
| 1             | P : 14.000            | 10.500     | 10.500      | 0.210    | 0.210    | 0.350    | 0.350    | 0.210    | 0.035     | 0.035     |
|               | T : 7.000             | 7.000      | 7.000       | 0.420    | 0.980    | 0.350    | 0.350    | 0.210    | 1.400     | 0.350     |
|               | T : 17.500            | 17.500     | 17.500      | 0.630    | 1.190    | 0.700    | 0.700    | 0.420    | 1.435     | 0.185     |
| 2             | P : 14.000            | 10.500     | 10.500      | 0.210    | 0.210    | 0.350    | 0.350    | 0.210    | 0.035     | 0.035     |
|               | T : 7.000             | 7.000      | 7.000       | 0.420    | 0.980    | 0.350    | 0.350    | 0.210    | 1.400     | 0.350     |
|               | T : 17.500            | 17.500     | 17.500      | 0.630    | 1.190    | 0.700    | 0.700    | 0.420    | 1.435     | 0.185     |
| 3             | P : 15.930            | 11.593     | 11.593      | 0.270    | 0.232    | 0.418    | 0.403    | 0.251    | 0.039     | 0.039     |
|               | T : 7.145             | 7.145      | 7.145       | 0.422    | 1.000    | 0.352    | 0.354    | 0.211    | 1.429     | 0.357     |
|               | T : 18.738            | 18.738     | 18.738      | 0.693    | 1.232    | 0.770    | 0.758    | 0.462    | 1.468     | 0.396     |
| 4             | P : 4.976             | 3.621      | 3.621       | 0.094    | 0.072    | 0.131    | 0.126    | 0.078    | 0.012     | 0.012     |
|               | T : 7.109             | 7.109      | 7.109       | 0.420    | 0.295    | 0.350    | 0.353    | 0.210    | 1.422     | 0.355     |
|               | T : 10.730            | 10.730     | 10.730      | 0.505    | 1.068    | 0.481    | 0.479    | 0.289    | 1.434     | 0.368     |
| 5             | P : 1.049             | 0.384      | 0.384       | 0.051    | 0.038    | 0.049    | 0.032    | 0.029    | 0.001     | 0.001     |
|               | T : 6.901             | 6.901      | 6.901       | 0.021    | 0.979    | 0.017    | 0.173    | 0.010    | 1.398     | 0.350     |
|               | T : 7.375             | 7.375      | 7.375       | 0.072    | 0.986    | 0.066    | 0.205    | 0.040    | 1.399     | 0.351     |
| 6             | P : 10.954            | 7.971      | 7.971       | 0.185    | 0.159    | 0.288    | 0.277    | 0.173    | 0.027     | 0.027     |
|               | T : 8.037             | 8.037      | 8.037       | 0.002    | 0.005    | 0.002    | 0.002    | 0.001    | 0.007     | 0.002     |
|               | T : 8.098             | 8.098      | 8.098       | 0.188    | 0.165    | 0.290    | 0.279    | 0.174    | 0.034     | 0.028     |
| 7             | P : 8.843             | 3.237      | 3.237       | 0.432    | 0.065    | 0.414    | 0.270    | 0.249    | 0.011     | 0.011     |
|               | T : 0.118             | 0.000      | 0.000       | 0.000    | 0.011    | 0.000    | 0.003    | 0.000    | 0.024     | 0.005     |
|               | T : 3.355             | 3.355      | 3.355       | 0.433    | 0.081    | 0.415    | 0.273    | 0.249    | 0.034     | 0.017     |
| 8             | P : 12.797            | 11.209     | 11.209      | 0.618    | 0.224    | 0.702    | 0.548    | 0.421    | 0.037     | 0.037     |
|               | T : 0.154             | 0.003      | 0.003       | 0.003    | 0.022    | 0.002    | 0.005    | 0.001    | 0.031     | 0.003     |
|               | T : 11.363            | 11.363     | 11.363      | 0.621    | 0.246    | 0.704    | 0.552    | 0.422    | 0.069     | 0.045     |
| 9             | P : 18.807            | 10.649     | 10.649      | 0.587    | 0.213    | 0.667    | 0.520    | 0.400    | 0.035     | 0.035     |
|               | T : 0.038             | 0.001      | 0.001       | 0.001    | 0.005    | 0.001    | 0.003    | 0.003    | 0.008     | 0.002     |
|               | T : 10.685            | 10.685     | 10.685      | 0.588    | 0.218    | 0.667    | 0.521    | 0.400    | 0.043     | 0.037     |
| 10            | P : 0.990             | 0.569      | 0.569       | 0.031    | 0.011    | 0.035    | 0.027    | 0.021    | 0.002     | 0.002     |
|               | T : 0.117             | 0.002      | 0.002       | 0.002    | 0.016    | 0.002    | 0.004    | 0.001    | 0.023     | 0.005     |
|               | T : 0.677             | 0.677      | 0.677       | 0.033    | 0.028    | 0.037    | 0.031    | 0.022    | 0.025     | 0.008     |



BASE RATE TABLE  
=====

TIME INTERVAL: HOUR

PARAMETERS

| STREAM NUMBER | SS (KG/H) | VSS (KG/H) | ROSET (KG/H) | P (KG/H) | N (KG/H) | CD (G/H) | IG (G/H) | PR (G/H) | CA (KG/H) | MG (KG/H) |
|---------------|-----------|------------|--------------|----------|----------|----------|----------|----------|-----------|-----------|
| 11            | 0.940     | 0.532      | 0.532        | 0.029    | 0.011    | 0.033    | 0.026    | 0.020    | 0.002     | 0.002     |
| D             |           |            |              | 0.000    | 0.004    | 0.000    | 0.001    | 0.000    | 0.006     | 0.001     |
| T             |           |            |              | 0.000    | 0.015    | 0.034    | 0.027    | 0.020    | 0.008     | 0.003     |
| 12            | 17.867    | 10.115     | 10.115       | 0.558    | 0.202    | 0.634    | 0.494    | 0.390    | 0.034     | 0.034     |
| D             |           |            |              | 0.000    | 0.001    | 0.000    | 0.000    | 0.000    | 0.002     | 0.000     |
| T             |           |            |              | 0.558    | 0.204    | 0.634    | 0.495    | 0.385    | 0.036     | 0.034     |
| 13            | 1.930     | 1.093      | 1.093        | 0.060    | 0.022    | 0.068    | 0.053    | 0.041    | 0.004     | 0.004     |
| D             |           |            |              | 0.002    | 0.020    | 0.002    | 0.004    | 0.001    | 0.020     | 0.007     |
| T             |           |            |              | 0.063    | 0.042    | 0.070    | 0.058    | 0.042    | 0.033     | 0.011     |
| STREAM NUMBER | SS (KG/H) | VSS (KG/H) | ROSET (KG/H) | P (KG/H) | N (KG/H) | CD (G/H) | IG (G/H) | PR (G/H) | CA (KG/H) | MG (KG/H) |

NIVA - PREDEF5

DATE: 1980-03-28

TIME: 00.15.12

PAGE: 4

MASS RATE TABLE

TIME INTERVAL: DAY

PARAMETERS

| STREAM NUMBER | SS (KG/D) | VSS (KG/D) | BPE7 (KG/D) | P (KG/D) | N (KG/D) | CD (G/D) | HG (G/D) | DR (G/D) | CA (KG/D) | MG (KG/D) |
|---------------|-----------|------------|-------------|----------|----------|----------|----------|----------|-----------|-----------|
| 1             | P 336.000 | 252.000    | 252.000     | 5.040    | 5.040    | 8.400    | 8.400    | 5.040    | 0.840     | 0.840     |
|               | U 168.000 | 168.000    | 168.000     | 10.080   | 23.520   | 8.400    | 8.400    | 5.040    | 33.600    | 8.400     |
|               | T 420.000 | 420.000    | 420.000     | 15.120   | 28.560   | 16.800   | 16.800   | 10.080   | 34.440    | 9.240     |
| 2             | P 336.000 | 252.000    | 252.000     | 5.040    | 5.040    | 8.400    | 8.400    | 5.040    | 0.840     | 0.840     |
|               | U 168.000 | 168.000    | 168.000     | 10.080   | 23.520   | 8.400    | 8.400    | 5.040    | 33.600    | 8.400     |
|               | T 420.000 | 420.000    | 420.000     | 15.120   | 28.560   | 16.800   | 16.800   | 10.080   | 34.440    | 9.240     |
| 3             | P 382.325 | 278.229    | 278.229     | 6.487    | 5.565    | 10.043   | 9.682    | 6.026    | 0.927     | 0.927     |
|               | U 171.492 | 171.492    | 171.492     | 10.137   | 24.009   | 8.447    | 8.507    | 5.068    | 34.208    | 8.575     |
|               | T 449.721 | 449.721    | 449.721     | 16.623   | 29.573   | 18.490   | 18.189   | 11.094   | 35.226    | 9.502     |
| 4             | P 119.431 | 86.913     | 86.913      | 2.926    | 1.738    | 3.137    | 3.024    | 1.882    | 0.290     | 0.290     |
|               | U 170.615 | 170.615    | 170.615     | 10.085   | 23.886   | 8.404    | 8.464    | 5.042    | 34.123    | 8.531     |
|               | T 257.529 | 257.529    | 257.529     | 12.111   | 25.624   | 11.541   | 11.488   | 6.925    | 34.413    | 8.870     |
| 5             | P 25.148  | 9.214      | 9.214       | 1.230    | 0.184    | 1.179    | 0.769    | 0.707    | 0.031     | 0.031     |
|               | U 167.786 | 167.786    | 167.786     | 0.466    | 23.490   | 0.413    | 4.162    | 0.248    | 33.557    | 8.389     |
|               | T 176.999 | 176.999    | 176.999     | 1.726    | 23.674   | 1.592    | 4.931    | 0.955    | 33.588    | 8.420     |
| 6             | P 262.894 | 191.316    | 191.316     | 4.460    | 3.826    | 6.906    | 6.657    | 4.143    | 0.438     | 0.438     |
|               | U 0.876   | 0.876      | 0.876       | 0.052    | 0.123    | 0.043    | 0.043    | 0.026    | 0.175     | 0.044     |
|               | T 192.102 | 192.102    | 192.102     | 4.512    | 3.949    | 6.949    | 6.701    | 4.169    | 0.613     | 0.613     |
| 7             | P 212.241 | 177.699    | 177.699     | 10.376   | 1.554    | 9.942    | 6.487    | 5.965    | 0.259     | 0.259     |
|               | U 2.830   | 2.830      | 2.830       | 0.008    | 0.366    | 0.007    | 0.070    | 0.004    | 0.566     | 0.141     |
|               | T 80.529  | 80.529     | 80.529      | 10.385   | 1.950    | 9.949    | 6.557    | 5.969    | 0.825     | 0.400     |
| 8             | P 475.135 | 269.015    | 269.015     | 14.837   | 5.380    | 16.848   | 13.144   | 10.109   | 0.807     | 0.877     |
|               | U 3.706   | 3.706      | 3.706       | 0.060    | 0.519    | 0.050    | 0.114    | 0.030    | 0.741     | 0.185     |
|               | T 272.721 | 272.721    | 272.721     | 14.897   | 5.899    | 16.898   | 13.258   | 10.139   | 1.638     | 1.092     |
| 9             | P 451.378 | 255.564    | 255.564     | 14.005   | 5.111    | 16.005   | 12.487   | 9.603    | 0.852     | 0.852     |
|               | U 0.903   | 0.903      | 0.903       | 0.015    | 0.126    | 0.012    | 0.028    | 0.007    | 0.181     | 0.045     |
|               | T 256.467 | 256.467    | 256.467     | 14.110   | 5.238    | 16.017   | 12.515   | 9.610    | 1.032     | 0.897     |
| 10            | P 23.757  | 13.451     | 13.451      | 0.742    | 0.269    | 0.842    | 0.657    | 0.505    | 0.045     | 0.045     |
|               | U 2.803   | 2.803      | 2.803       | 0.046    | 0.302    | 0.038    | 0.086    | 0.023    | 0.561     | 0.140     |
|               | T 16.254  | 16.254     | 16.254      | 0.787    | 0.661    | 0.880    | 0.743    | 0.528    | 0.606     | 0.185     |



MASS RATE TABLE

TIME INTERVAL: YEAR

| STREAM NUMBER | PARAMETERS |             |              |           |           |           |           |           |            |            |            |             |              |           |           |           |           |           |            |            |       |       |
|---------------|------------|-------------|--------------|-----------|-----------|-----------|-----------|-----------|------------|------------|------------|-------------|--------------|-----------|-----------|-----------|-----------|-----------|------------|------------|-------|-------|
|               | SS (TON/Y) | VSS (TON/Y) | BOF7 (TON/Y) | P (TON/Y) | N (TON/Y) | CD (KG/Y) | HC (KG/Y) | PB (KG/Y) | CA (TON/Y) | WG (TON/Y) | SS (TON/Y) | VSS (TON/Y) | BOF7 (TON/Y) | P (TON/Y) | N (TON/Y) | CD (KG/Y) | HC (KG/Y) | PB (KG/Y) | CA (TON/Y) | WG (TON/Y) |       |       |
| 1             | P          | 122.640     | 91.090       | 91.980    | 1.840     | 1.840     | 3.066     | 3.066     | 1.840      | 0.307      | 0.307      | 3.066       | 3.066        | 1.840     | 1.840     | 3.066     | 3.066     | 1.840     | 0.307      | 0.307      | 3.066 | 3.066 |
|               | D          |             |              | 61.320    | 3.679     | 8.585     | 3.066     | 3.066     | 1.840      | 1.840      | 1.840      | 3.066       | 3.066        | 1.840     | 1.840     | 3.066     | 3.066     | 1.840     | 0.307      | 0.307      | 3.066 | 3.066 |
|               | T          |             |              | 153.300   | 5.519     | 10.424    | 6.132     | 6.132     | 3.679      | 3.679      | 3.679      | 6.132       | 6.132        | 5.519     | 5.519     | 6.132     | 6.132     | 3.679     | 12.571     | 12.571     | 6.132 | 6.132 |
| 2             | P          | 122.640     | 91.090       | 91.980    | 1.840     | 1.840     | 3.066     | 3.066     | 1.840      | 0.307      | 0.307      | 3.066       | 3.066        | 1.840     | 1.840     | 3.066     | 3.066     | 1.840     | 0.307      | 0.307      | 3.066 | 3.066 |
|               | D          |             |              | 61.320    | 3.679     | 8.585     | 3.066     | 3.066     | 1.840      | 1.840      | 1.840      | 3.066       | 3.066        | 1.840     | 1.840     | 3.066     | 3.066     | 1.840     | 0.307      | 0.307      | 3.066 | 3.066 |
|               | T          |             |              | 153.300   | 5.519     | 10.424    | 6.132     | 6.132     | 3.679      | 3.679      | 3.679      | 6.132       | 6.132        | 5.519     | 5.519     | 6.132     | 6.132     | 3.679     | 12.571     | 12.571     | 6.132 | 6.132 |
| 3             | P          | 132.549     | 101.553      | 101.553   | 2.368     | 2.368     | 3.666     | 3.666     | 2.031      | 0.330      | 0.330      | 3.666       | 3.666        | 2.368     | 2.368     | 3.666     | 3.666     | 2.031     | 0.330      | 0.330      | 3.666 | 3.666 |
|               | D          |             |              | 62.504    | 3.700     | 9.743     | 3.666     | 3.666     | 2.031      | 2.031      | 2.031      | 3.666       | 3.666        | 3.700     | 3.700     | 3.666     | 3.666     | 2.031     | 12.519     | 12.519     | 3.666 | 3.666 |
|               | T          |             |              | 164.148   | 6.067     | 10.794    | 6.749     | 6.749     | 4.040      | 4.040      | 4.040      | 6.749       | 6.749        | 6.067     | 6.067     | 6.749     | 6.749     | 4.040     | 12.857     | 12.857     | 6.749 | 6.749 |
| 4             | P          | 43.593      | 31.723       | 31.723    | 0.740     | 0.740     | 1.145     | 1.145     | 0.634      | 0.104      | 0.104      | 1.145       | 1.145        | 0.740     | 0.740     | 1.145     | 1.145     | 0.634     | 0.104      | 0.104      | 1.145 | 1.145 |
|               | D          |             |              | 62.275    | 3.981     | 8.718     | 3.067     | 3.067     | 1.840      | 1.840      | 1.840      | 3.067       | 3.067        | 3.981     | 3.981     | 3.067     | 3.067     | 1.840     | 12.455     | 12.455     | 3.067 | 3.067 |
|               | T          |             |              | 93.998    | 4.421     | 9.333     | 4.213     | 4.213     | 4.103      | 4.103      | 4.103      | 4.213       | 4.213        | 4.421     | 4.421     | 4.213     | 4.213     | 4.103     | 12.561     | 12.561     | 4.213 | 4.213 |
| 5             | P          | 9.186       | 3.363        | 3.363     | 0.449     | 0.449     | 0.430     | 0.430     | 0.097      | 0.011      | 0.011      | 0.430       | 0.430        | 0.449     | 0.449     | 0.430     | 0.430     | 0.097     | 0.011      | 0.011      | 0.430 | 0.430 |
|               | D          |             |              | 61.242    | 0.181     | 8.574     | 0.151     | 0.151     | 1.519      | 1.519      | 1.519      | 0.151       | 0.151        | 61.242    | 61.242    | 0.151     | 0.151     | 1.519     | 12.248     | 12.248     | 0.151 | 0.151 |
|               | T          |             |              | 64.605    | 0.630     | 8.641     | 0.581     | 0.581     | 1.800      | 1.800      | 1.800      | 0.581       | 0.581        | 64.605    | 64.605    | 0.581     | 0.581     | 1.800     | 12.260     | 12.260     | 0.581 | 0.581 |
| 6             | P          | 95.956      | 69.830       | 69.830    | 1.628     | 1.628     | 2.521     | 2.521     | 1.397      | 0.233      | 0.233      | 2.521       | 2.521        | 1.628     | 1.628     | 2.521     | 2.521     | 1.397     | 0.233      | 0.233      | 2.521 | 2.521 |
|               | D          |             |              | 1.033     | 0.003     | 0.019     | 0.016     | 0.016     | 0.045      | 0.045      | 0.045      | 0.016       | 0.016        | 1.033     | 1.033     | 0.016     | 0.016     | 0.045     | 0.045      | 0.045      | 0.016 | 0.016 |
|               | T          |             |              | 70.150    | 1.647     | 1.441     | 2.536     | 2.536     | 1.441      | 1.441      | 1.441      | 2.536       | 2.536        | 1.647     | 1.647     | 2.536     | 2.536     | 1.441     | 0.297      | 0.297      | 2.536 | 2.536 |
| 7             | P          | 77.468      | 28.360       | 28.360    | 3.787     | 3.787     | 3.629     | 3.629     | 0.567      | 0.095      | 0.095      | 3.629       | 3.629        | 3.787     | 3.787     | 3.629     | 3.629     | 0.567     | 0.095      | 0.095      | 3.629 | 3.629 |
|               | D          |             |              | 1.033     | 0.003     | 0.019     | 0.003     | 0.003     | 0.145      | 0.145      | 0.145      | 0.003       | 0.003        | 1.033     | 1.033     | 0.003     | 0.003     | 0.145     | 0.207      | 0.207      | 0.003 | 0.003 |
|               | T          |             |              | 29.393    | 3.790     | 0.712     | 3.631     | 3.631     | 0.712      | 0.712      | 0.712      | 3.631       | 3.631        | 29.393    | 29.393    | 0.712     | 0.712     | 3.631     | 0.301      | 0.301      | 3.631 | 3.631 |
| 8             | P          | 173.424     | 98.190       | 98.190    | 5.415     | 5.415     | 6.149     | 6.149     | 1.964      | 0.327      | 0.327      | 6.149       | 6.149        | 5.415     | 5.415     | 6.149     | 6.149     | 1.964     | 0.327      | 0.327      | 6.149 | 6.149 |
|               | D          |             |              | 1.353     | 0.022     | 0.189     | 0.041     | 0.041     | 0.041      | 0.041      | 0.041      | 0.041       | 0.041        | 1.353     | 1.353     | 0.041     | 0.041     | 0.041     | 0.271      | 0.271      | 0.041 | 0.041 |
|               | T          |             |              | 99.543    | 5.437     | 2.153     | 6.148     | 6.148     | 2.153      | 2.153      | 2.153      | 6.148       | 6.148        | 99.543    | 99.543    | 2.153     | 6.148     | 6.148     | 0.568      | 0.568      | 6.148 | 6.148 |
| 9             | P          | 164.753     | 93.281       | 93.281    | 5.145     | 5.145     | 5.842     | 5.842     | 1.866      | 0.311      | 0.311      | 5.842       | 5.842        | 5.145     | 5.145     | 5.842     | 5.842     | 1.866     | 0.311      | 0.311      | 5.842 | 5.842 |
|               | D          |             |              | 0.330     | 0.005     | 0.005     | 0.004     | 0.004     | 0.004      | 0.004      | 0.004      | 0.004       | 0.004        | 0.330     | 0.330     | 0.004     | 0.004     | 0.004     | 0.004      | 0.004      | 0.004 | 0.004 |
|               | T          |             |              | 93.610    | 5.150     | 1.912     | 5.846     | 5.846     | 1.912      | 1.912      | 1.912      | 5.846       | 5.846        | 93.610    | 93.610    | 1.912     | 5.846     | 5.846     | 0.317      | 0.317      | 5.846 | 5.846 |
| 10            | P          | 9.671       | 4.910        | 4.910     | 0.271     | 0.271     | 0.307     | 0.307     | 0.240      | 0.016      | 0.016      | 0.307       | 0.307        | 4.910     | 4.910     | 0.307     | 0.307     | 0.240     | 0.016      | 0.016      | 0.307 | 0.307 |
|               | D          |             |              | 1.023     | 0.017     | 0.143     | 0.014     | 0.014     | 0.031      | 0.031      | 0.031      | 0.014       | 0.014        | 1.023     | 1.023     | 0.014     | 0.014     | 0.031     | 0.205      | 0.205      | 0.014 | 0.014 |
|               | T          |             |              | 5.933     | 0.287     | 0.241     | 0.321     | 0.321     | 0.241      | 0.241      | 0.241      | 0.321       | 0.321        | 5.933     | 5.933     | 0.241     | 0.321     | 0.241     | 0.205      | 0.205      | 0.321 | 0.321 |



ITERATION TABLE

PARAMETER NAME: 0 (M3/H)

| STREAM NUMBER | ITERATION NUMBER |        |        |        |        |        |        | RELATIVE DIFFERENCE (%) |
|---------------|------------------|--------|--------|--------|--------|--------|--------|-------------------------|
|               | 1                | 2      | 3      | 4      | 5      | 6      | 7      |                         |
| 1             | 70.000           | 70.000 | 70.000 | 70.000 | 70.000 | 70.000 | 70.000 | 0.00                    |
| 2             | 0.000            | 70.000 | 70.000 | 70.000 | 70.000 | 70.000 | 70.000 | 0.00                    |
| 3             | 0.000            | 70.000 | 71.398 | 71.449 | 71.454 | 71.455 | 71.455 | 0.00                    |
| 4             | 0.000            | 69.696 | 71.030 | 71.084 | 71.090 | 71.090 | 71.090 | 0.00                    |
| 5             | 0.000            | 68.521 | 69.861 | 69.905 | 69.910 | 69.911 | 69.911 | 0.00                    |
| 6             | 0.000            | 0.304  | 0.352  | 0.365  | 0.365  | 0.365  | 0.365  | 0.00                    |
| 7             | 0.000            | 1.175  | 1.178  | 1.179  | 1.179  | 1.179  | 1.179  | 0.00                    |
| 8             | 0.000            | 1.479  | 1.537  | 1.544  | 1.544  | 1.544  | 1.544  | 0.00                    |
| 9             | 0.000            | 0.341  | 0.373  | 0.376  | 0.376  | 0.376  | 0.376  | 0.00                    |
| 10            | 0.000            | 1.138  | 1.165  | 1.168  | 1.168  | 1.168  | 1.168  | 0.00                    |
| 11            | 0.000            | 0.260  | 0.284  | 0.287  | 0.287  | 0.287  | 0.287  | 0.00                    |
| 12            | 0.000            | 0.081  | 0.089  | 0.089  | 0.089  | 0.089  | 0.089  | 0.00                    |
| 13            | 0.000            | 1.398  | 1.449  | 1.454  | 1.455  | 1.455  | 1.455  | 0.00                    |

NVA - PREDES

DATE: 1980-03-28

TIME: 00.15.12

PAGE: 11

ITERATION TABLE

PARAMETER NAME: SS/P (KG/M3)

| STREAM NUMBER | 1     | 2       | 3       | 4       | 5       | 6       | 7       | RELATIVE DIFFERENCE (%) |
|---------------|-------|---------|---------|---------|---------|---------|---------|-------------------------|
| 1             | 0.000 | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.00                    |
| 2             | 0.000 | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.00                    |
| 3             | 0.000 | 0.200   | 0.221   | 0.223   | 0.223   | 0.223   | 0.223   | 0.00                    |
| 4             | 0.000 | 0.070   | 0.070   | 0.070   | 0.070   | 0.070   | 0.070   | 0.00                    |
| 5             | 0.000 | 0.015   | 0.015   | 0.015   | 0.015   | 0.015   | 0.015   | 0.00                    |
| 6             | 0.000 | 30.000  | 30.000  | 30.000  | 30.000  | 30.000  | 30.000  | 0.00                    |
| 7             | 0.000 | 7.500   | 7.500   | 7.500   | 7.500   | 7.500   | 7.500   | 0.00                    |
| 8             | 0.000 | 12.125  | 12.757  | 12.814  | 12.810  | 12.420  | 12.820  | 0.00                    |
| 9             | 0.000 | 50.000  | 50.000  | 50.000  | 50.000  | 50.000  | 50.000  | 0.00                    |
| 10            | 0.000 | 0.788   | 0.842   | 0.847   | 0.847   | 0.847   | 0.847   | 0.00                    |
| 11            | 0.000 | 3.270   | 3.270   | 3.270   | 3.270   | 3.270   | 3.270   | 0.00                    |
| 12            | 0.000 | 200.000 | 200.000 | 200.000 | 200.000 | 200.000 | 200.000 | 0.00                    |
| 13            | 0.000 | 1.251   | 1.320   | 1.326   | 1.327   | 1.327   | 1.327   | 0.00                    |

| STREAM NUMBER | 1     | 2       | 3       | 4       | 5       | 6       | 7       | RELATIVE DIFFERENCE (%) |
|---------------|-------|---------|---------|---------|---------|---------|---------|-------------------------|
| 1             | 0.000 | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.00                    |
| 2             | 0.000 | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.200   | 0.00                    |
| 3             | 0.000 | 0.200   | 0.221   | 0.223   | 0.223   | 0.223   | 0.223   | 0.00                    |
| 4             | 0.000 | 0.070   | 0.070   | 0.070   | 0.070   | 0.070   | 0.070   | 0.00                    |
| 5             | 0.000 | 0.015   | 0.015   | 0.015   | 0.015   | 0.015   | 0.015   | 0.00                    |
| 6             | 0.000 | 30.000  | 30.000  | 30.000  | 30.000  | 30.000  | 30.000  | 0.00                    |
| 7             | 0.000 | 7.500   | 7.500   | 7.500   | 7.500   | 7.500   | 7.500   | 0.00                    |
| 8             | 0.000 | 12.125  | 12.757  | 12.814  | 12.810  | 12.420  | 12.820  | 0.00                    |
| 9             | 0.000 | 50.000  | 50.000  | 50.000  | 50.000  | 50.000  | 50.000  | 0.00                    |
| 10            | 0.000 | 0.788   | 0.842   | 0.847   | 0.847   | 0.847   | 0.847   | 0.00                    |
| 11            | 0.000 | 3.270   | 3.270   | 3.270   | 3.270   | 3.270   | 3.270   | 0.00                    |
| 12            | 0.000 | 200.000 | 200.000 | 200.000 | 200.000 | 200.000 | 200.000 | 0.00                    |
| 13            | 0.000 | 1.251   | 1.320   | 1.326   | 1.327   | 1.327   | 1.327   | 0.00                    |

ITERATION TABLE

PARAMETER NAME: VSS/P (KC/M3)

| STREAM NUMBER | ITERATION NUMBER |         |         |         |         |         |         | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---------|---------|---------|---------|---------|---------|-------------------------|
|               | 1                | 2       | 3       | 4       | 5       | 6       | 7       |                         |
| 1             | 0.150            | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.00                    |
| 2             | 0.000            | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.00                    |
| 3             | 0.000            | 0.150   | 0.161   | 0.162   | 0.162   | 0.162   | 0.162   | 0.00                    |
| 4             | 0.000            | 0.052   | 0.051   | 0.051   | 0.051   | 0.051   | 0.051   | 0.00                    |
| 5             | 0.000            | 0.006   | 0.006   | 0.005   | 0.005   | 0.005   | 0.005   | 0.00                    |
| 6             | 0.000            | 22.500  | 21.681  | 21.837  | 21.832  | 21.832  | 21.832  | 0.00                    |
| 7             | 0.000            | 2.789   | 2.752   | 2.746   | 2.746   | 2.746   | 2.746   | 0.00                    |
| 8             | 0.000            | 6.841   | 7.221   | 7.255   | 7.258   | 7.259   | 7.259   | 0.00                    |
| 9             | 0.000            | 28.210  | 28.303  | 28.309  | 28.309  | 28.309  | 28.309  | 0.00                    |
| 10            | 0.000            | 0.444   | 0.477   | 0.479   | 0.480   | 0.480   | 0.480   | 0.00                    |
| 11            | 0.000            | 1.950   | 1.856   | 1.856   | 1.856   | 1.856   | 1.856   | 0.00                    |
| 12            | 0.000            | 112.839 | 113.211 | 113.236 | 113.237 | 113.237 | 113.237 | 0.00                    |
| 13            | 0.000            | 0.706   | 0.747   | 0.751   | 0.751   | 0.751   | 0.751   | 0.00                    |



ITERATION TABLE

PARAMETER NAME: BOF7/P (KG/H3)

| STREAM NUMBER | ITERATION NUMBER |         |         |         |         |         |         | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---------|---------|---------|---------|---------|---------|-------------------------|
|               | 1                | 2       | 3       | 4       | 5       | 6       | 7       |                         |
| 1             | 0.150            | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.00                    |
| 2             | 0.000            | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.00                    |
| 3             | 0.000            | 0.150   | 0.161   | 0.162   | 0.162   | 0.162   | 0.162   | 0.00                    |
| 4             | 0.000            | 0.052   | 0.051   | 0.051   | 0.051   | 0.051   | 0.051   | 0.00                    |
| 5             | 0.000            | 0.006   | 0.005   | 0.005   | 0.005   | 0.005   | 0.005   | 0.00                    |
| 6             | 0.000            | 22.500  | 21.881  | 21.837  | 21.832  | 21.832  | 21.832  | 0.00                    |
| 7             | 0.000            | 2.789   | 2.752   | 2.746   | 2.746   | 2.746   | 2.746   | 0.00                    |
| 8             | 0.000            | 6.841   | 7.221   | 7.255   | 7.258   | 7.258   | 7.259   | 0.00                    |
| 9             | 0.000            | 28.210  | 28.303  | 28.309  | 28.309  | 28.309  | 28.309  | 0.00                    |
| 10            | 0.000            | 0.444   | 0.477   | 0.479   | 0.480   | 0.480   | 0.480   | 0.00                    |
| 11            | 0.000            | 1.850   | 1.856   | 1.856   | 1.856   | 1.856   | 1.856   | 0.00                    |
| 12            | 0.000            | 112.839 | 113.211 | 113.236 | 113.237 | 113.237 | 113.237 | 0.00                    |
| 13            | 0.000            | 0.706   | 0.747   | 0.751   | 0.751   | 0.751   | 0.751   | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |         |         |         |         |         |         | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---------|---------|---------|---------|---------|---------|-------------------------|
|               | 1                | 2       | 3       | 4       | 5       | 6       | 7       |                         |
| 1             | 0.150            | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.00                    |
| 2             | 0.000            | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.150   | 0.00                    |
| 3             | 0.000            | 0.150   | 0.161   | 0.162   | 0.162   | 0.162   | 0.162   | 0.00                    |
| 4             | 0.000            | 0.052   | 0.051   | 0.051   | 0.051   | 0.051   | 0.051   | 0.00                    |
| 5             | 0.000            | 0.006   | 0.005   | 0.005   | 0.005   | 0.005   | 0.005   | 0.00                    |
| 6             | 0.000            | 22.500  | 21.881  | 21.837  | 21.832  | 21.832  | 21.832  | 0.00                    |
| 7             | 0.000            | 2.789   | 2.752   | 2.746   | 2.746   | 2.746   | 2.746   | 0.00                    |
| 8             | 0.000            | 6.841   | 7.221   | 7.255   | 7.258   | 7.258   | 7.259   | 0.00                    |
| 9             | 0.000            | 28.210  | 28.303  | 28.309  | 28.309  | 28.309  | 28.309  | 0.00                    |
| 10            | 0.000            | 0.444   | 0.477   | 0.479   | 0.480   | 0.480   | 0.480   | 0.00                    |
| 11            | 0.000            | 1.850   | 1.856   | 1.856   | 1.856   | 1.856   | 1.856   | 0.00                    |
| 12            | 0.000            | 112.839 | 113.211 | 113.236 | 113.237 | 113.237 | 113.237 | 0.00                    |
| 13            | 0.000            | 0.706   | 0.747   | 0.751   | 0.751   | 0.751   | 0.751   | 0.00                    |

VIVA - PREDICS

DATE: 1090-03-28

TIME: 00.15.12

PAGE: 14

ITERATION TABLE

PARAMETER NAME: P/P (KG/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.003            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 2             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 3             | 0.000            | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.00                    |
| 4             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 5             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 6             | 0.000            | 0.450 | 0.504 | 0.503 | 0.500 | 0.500 | 0.500 | 0.00                    |
| 7             | 0.000            | 0.359 | 0.366 | 0.367 | 0.367 | 0.367 | 0.367 | 0.00                    |
| 8             | 0.000            | 0.377 | 0.392 | 0.400 | 0.400 | 0.400 | 0.400 | 0.00                    |
| 9             | 0.000            | 1.556 | 1.561 | 1.561 | 1.561 | 1.561 | 1.561 | 0.00                    |
| 10            | 0.000            | 0.025 | 0.025 | 0.026 | 0.026 | 0.026 | 0.026 | 0.00                    |
| 11            | 0.000            | 0.102 | 0.102 | 0.102 | 0.102 | 0.102 | 0.102 | 0.00                    |
| 12            | 0.000            | 6.224 | 6.243 | 6.245 | 6.245 | 6.245 | 6.245 | 0.00                    |
| 13            | 0.000            | 0.030 | 0.041 | 0.041 | 0.041 | 0.041 | 0.041 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |   |   |   |   |   |   | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---|---|---|---|---|---|-------------------------|
|               | 1                | 2 | 3 | 4 | 5 | 6 | 7 |                         |
| 1             |                  |   |   |   |   |   |   |                         |
| 2             |                  |   |   |   |   |   |   |                         |
| 3             |                  |   |   |   |   |   |   |                         |
| 4             |                  |   |   |   |   |   |   |                         |
| 5             |                  |   |   |   |   |   |   |                         |
| 6             |                  |   |   |   |   |   |   |                         |
| 7             |                  |   |   |   |   |   |   |                         |

ITERATION TABLE

PARAMETER NAME: N/P (KG/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.003            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 2             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 3             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 4             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 5             | 0.000            | 0.030 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.450 | 0.438 | 0.437 | 0.437 | 0.437 | 0.437 | 0.00                    |
| 7             | 0.000            | 0.056 | 0.055 | 0.055 | 0.055 | 0.055 | 0.055 | 0.00                    |
| 8             | 0.000            | 0.137 | 0.144 | 0.145 | 0.145 | 0.145 | 0.145 | 0.00                    |
| 9             | 0.000            | 0.564 | 0.566 | 0.566 | 0.566 | 0.566 | 0.566 | 0.00                    |
| 10            | 0.000            | 0.009 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 | 0.00                    |
| 11            | 0.000            | 0.037 | 0.037 | 0.037 | 0.037 | 0.037 | 0.037 | 0.00                    |
| 12            | 0.000            | 2.257 | 2.264 | 2.265 | 2.265 | 2.265 | 2.265 | 0.00                    |
| 13            | 0.000            | 0.014 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 | 0.00                    |

VIVA - PINDES

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 16

ITERATION TABLE

PARAMETER NAME: CD/P (G/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.000            | 0.005 | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 4             | 0.000            | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 5             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 6             | 0.000            | 0.750 | 0.784 | 0.788 | 0.788 | 0.788 | 0.788 | 0.00                    |
| 7             | 0.000            | 0.345 | 0.351 | 0.351 | 0.351 | 0.351 | 0.351 | 0.00                    |
| 8             | 0.000            | 0.428 | 0.452 | 0.454 | 0.455 | 0.455 | 0.455 | 0.00                    |
| 9             | 0.000            | 1.767 | 1.772 | 1.773 | 1.773 | 1.773 | 1.773 | 0.00                    |
| 10            | 0.000            | 0.028 | 0.030 | 0.030 | 0.030 | 0.030 | 0.030 | 0.00                    |
| 11            | 0.000            | 0.116 | 0.116 | 0.116 | 0.116 | 0.116 | 0.116 | 0.00                    |
| 12            | 0.000            | 7.068 | 7.089 | 7.091 | 7.092 | 7.092 | 7.092 | 0.00                    |
| 13            | 0.000            | 0.044 | 0.047 | 0.047 | 0.047 | 0.047 | 0.047 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |   |   |   |   |   |   | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---|---|---|---|---|---|-------------------------|
|               | 1                | 2 | 3 | 4 | 5 | 6 | 7 |                         |
| 1             |                  |   |   |   |   |   |   |                         |
| 2             |                  |   |   |   |   |   |   |                         |
| 3             |                  |   |   |   |   |   |   |                         |
| 4             |                  |   |   |   |   |   |   |                         |
| 5             |                  |   |   |   |   |   |   |                         |
| 6             |                  |   |   |   |   |   |   |                         |
| 7             |                  |   |   |   |   |   |   |                         |

ITERATION TABLE

PARAMETER NAME: HIGZP (G/M3)

| SERIAL NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.000            | 0.005 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 4             | 0.000            | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 5             | 3.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.750 | 0.758 | 0.760 | 0.760 | 0.760 | 0.760 | 0.00                    |
| 7             | 0.000            | 0.226 | 0.229 | 0.229 | 0.229 | 0.229 | 0.229 | 0.00                    |
| 8             | 0.000            | 0.334 | 0.353 | 0.354 | 0.355 | 0.355 | 0.355 | 0.00                    |
| 9             | 0.000            | 1.375 | 1.383 | 1.383 | 1.383 | 1.383 | 1.383 | 0.00                    |
| 10            | 0.000            | 0.022 | 0.023 | 0.023 | 0.023 | 0.023 | 0.023 | 0.00                    |
| 11            | 0.000            | 0.090 | 0.091 | 0.091 | 0.091 | 0.091 | 0.091 | 0.00                    |
| 12            | 0.000            | 5.502 | 5.530 | 5.533 | 5.533 | 5.533 | 5.533 | 0.00                    |
| 13            | 0.000            | 0.034 | 0.036 | 0.037 | 0.037 | 0.037 | 0.037 | 0.00                    |

HIVA - PREPES

DATE: 1990-03-28

TIME: 09.15.12

PAGE: 18

ITERATION TABLE

PARAMETER NAME: PB/P (C/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.003            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 2             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 3             | 0.003            | 0.003 | 0.003 | 0.004 | 0.004 | 0.004 | 0.004 | 0.00                    |
| 4             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.450 | 0.471 | 0.473 | 0.473 | 0.473 | 0.473 | 0.00                    |
| 7             | 0.000            | 0.207 | 0.211 | 0.211 | 0.211 | 0.211 | 0.211 | 0.00                    |
| 8             | 0.000            | 0.257 | 0.271 | 0.273 | 0.273 | 0.273 | 0.273 | 0.00                    |
| 9             | 0.000            | 1.060 | 1.063 | 1.064 | 1.064 | 1.064 | 1.064 | 0.00                    |
| 10            | 0.000            | 0.017 | 0.018 | 0.018 | 0.018 | 0.018 | 0.018 | 0.00                    |
| 11            | 0.000            | 0.070 | 0.070 | 0.070 | 0.070 | 0.070 | 0.070 | 0.00                    |
| 12            | 0.000            | 4.241 | 4.254 | 4.255 | 4.255 | 4.255 | 4.255 | 0.00                    |
| 13            | 0.000            | 0.027 | 0.028 | 0.028 | 0.028 | 0.028 | 0.028 | 0.00                    |

NIVA - PREDIS

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 10

ITERATION TABLE

PARAMETER NAME: CA/P (KG/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 2             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 3             | 0.000            | 0.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 4             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.075 | 0.073 | 0.073 | 0.073 | 0.073 | 0.073 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 8             | 0.000            | 0.023 | 0.024 | 0.024 | 0.024 | 0.024 | 0.024 | 0.00                    |
| 9             | 0.000            | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.004 | 0.00                    |
| 10            | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 11            | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 12            | 0.000            | 0.376 | 0.377 | 0.377 | 0.377 | 0.377 | 0.377 | 0.00                    |
| 13            | 0.000            | 0.002 | 0.002 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |

QIVA - RWDF05

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 20

ITERATION TABLE

PARAMETER NAME: MG/P (KG/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 2             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 3             | 0.000            | 0.000 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 4             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.075 | 0.073 | 0.073 | 0.073 | 0.073 | 0.073 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 | 0.00                    |
| 8             | 0.000            | 0.000 | 0.023 | 0.024 | 0.024 | 0.024 | 0.024 | 0.00                    |
| 9             | 0.000            | 0.000 | 0.094 | 0.094 | 0.094 | 0.094 | 0.094 | 0.00                    |
| 10            | 0.000            | 0.000 | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 11            | 0.000            | 0.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 12            | 0.000            | 0.376 | 0.377 | 0.377 | 0.377 | 0.377 | 0.377 | 0.00                    |
| 13            | 0.000            | 0.002 | 0.002 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 2             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 3             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 4             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |

NIVA - PREPDS

DATE: 1980-03-28

TIME: 00.15.12

PAGE: 21



ITERATION TABLE

PARAMETER NAME: ROBE/1 (KG/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.100            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 2             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 3             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 4             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 5             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 6             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 7             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 8             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 9             | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 10            | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 11            | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 12            | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |
| 13            | 0.000            | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |   |   |   |   |   |   | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---|---|---|---|---|---|-------------------------|
|               | 1                | 2 | 3 | 4 | 5 | 6 | 7 |                         |
| 1             |                  |   |   |   |   |   |   |                         |
| 2             |                  |   |   |   |   |   |   |                         |
| 3             |                  |   |   |   |   |   |   |                         |
| 4             |                  |   |   |   |   |   |   |                         |
| 5             |                  |   |   |   |   |   |   |                         |
| 6             |                  |   |   |   |   |   |   |                         |
| 7             |                  |   |   |   |   |   |   |                         |

NIVA - GREENE

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 22

ITERATION TABLE

PARAMETER NAME: P/D (KG/W3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 2             | 0.000            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 3             | 0.005            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 4             | 0.000            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 8             | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 9             | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 10            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 11            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 12            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 13            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 2             | 0.000            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 3             | 0.005            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 4             | 0.000            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 8             | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 9             | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 10            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 11            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 12            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 13            | 0.000            | 0.001 | 0.002 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |

ITERATION TABLE

PARAMETER NAME: M/D (KG/W3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 2             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 3             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 4             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 5             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 6             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 7             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 8             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 9             | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 10            | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 11            | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 12            | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 13            | 0.000            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 2             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 3             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 4             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 5             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 6             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |
| 7             | 0.014            | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 | 0.00                    |

ITERATION TABLE

PARAMETER NAME: C10/D (G/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 4             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 5             | 0.000            | 0.005 | 0.005 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 8             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 9             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 10            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 11            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 12            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 13            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |

MVA - PREDES

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 25

ITERATION TABLE

PARAMETER NAME: HGL/D (G/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 4             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 5             | 0.000            | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 6             | 0.000            | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 7             | 0.000            | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 8             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 9             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 10            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 11            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 12            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 13            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 4             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 5             | 0.000            | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 6             | 0.000            | 0.003 | 0.003 | 0.002 | 0.002 | 0.002 | 0.002 | 0.00                    |
| 7             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 8             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 9             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 10            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 11            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 12            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 13            | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |

ITERATION TABLE

PARAMETER NAME: PH/D (G/M3)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.003            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 2             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 3             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 4             | 0.000            | 0.000 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 8             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 9             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 10            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 11            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 12            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 13            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.003            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 2             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 3             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 4             | 0.000            | 0.000 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 5             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 6             | 0.000            | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.003 | 0.00                    |
| 7             | 0.000            | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00                    |
| 8             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 9             | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 10            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 11            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 12            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |
| 13            | 0.000            | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.001 | 0.00                    |

NVA - PREDIC

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 27

ITERATION TABLE

PARAMETER NAME: CA/D (KG/M3)

| STREAM NUMBER | 1     | 2     | 3     | 4     | 5     | 6     | 7     | RELATIVE DIFFERENCE (%) |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------------------------|
| 1             | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 2             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 3             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 4             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 5             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 6             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 7             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 8             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 9             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 10            | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 11            | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 12            | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 13            | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |

| STREAM NUMBER | 1     | 2     | 3     | 4     | 5     | 6     | 7     | RELATIVE DIFFERENCE (%) |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------------------------|
| 1             | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 2             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 3             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 4             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 5             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 6             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |
| 7             | 0.000 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.020 | 0.00                    |

ITERATION TABLE

PARAMETER NAME: WC/D (KG/43)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 4             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 5             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 6             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 7             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 8             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 9             | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 10            | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 11            | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 12            | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 13            | 0.000            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 2             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 3             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 4             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 5             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 6             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |
| 7             | 0.005            | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.005 | 0.00                    |



\*\*\*\*\*  
 TO ORDER TABLE  
 \*\*\*\*\*

PARAMETER NAME: ALK/D (MEV.)

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 2.800            | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 0.00                    |
| 2             | 0.000            | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 0.00                    |
| 3             | 0.000            | 2.800 | 2.767 | 2.768 | 2.768 | 2.768 | 2.768 | 0.00                    |
| 4             | 0.000            | 2.800 | 2.767 | 2.768 | 2.768 | 2.768 | 2.768 | 0.00                    |
| 5             | 0.000            | 0.702 | 0.726 | 0.726 | 0.726 | 0.726 | 0.726 | 0.00                    |
| 6             | 0.000            | 2.800 | 2.767 | 2.768 | 2.768 | 2.768 | 2.768 | 0.00                    |
| 7             | 0.000            | 0.702 | 0.726 | 0.726 | 0.726 | 0.726 | 0.726 | 0.00                    |
| 8             | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 9             | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 10            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 11            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 12            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 13            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 2.800            | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 0.00                    |
| 2             | 0.000            | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 2.800 | 0.00                    |
| 3             | 0.000            | 2.800 | 2.767 | 2.768 | 2.768 | 2.768 | 2.768 | 0.00                    |
| 4             | 0.000            | 2.800 | 2.767 | 2.768 | 2.768 | 2.768 | 2.768 | 0.00                    |
| 5             | 0.000            | 0.702 | 0.726 | 0.726 | 0.726 | 0.726 | 0.726 | 0.00                    |
| 6             | 0.000            | 2.800 | 2.767 | 2.768 | 2.768 | 2.768 | 2.768 | 0.00                    |
| 7             | 0.000            | 0.702 | 0.726 | 0.726 | 0.726 | 0.726 | 0.726 | 0.00                    |
| 8             | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 9             | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 10            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 11            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 12            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |
| 13            | 0.000            | 1.133 | 1.203 | 1.208 | 1.209 | 1.209 | 1.209 | 0.00                    |

MIWA - PIERRES

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 30

ITERATION TABLE

PARAMETER NAME: PH2D

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 7.200            | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 0.00                    |
| 2             | 0.000            | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 0.00                    |
| 3             | 0.000            | 7.200 | 7.088 | 7.087 | 7.087 | 7.087 | 7.087 | 0.00                    |
| 4             | 0.000            | 7.200 | 7.088 | 7.087 | 7.087 | 7.087 | 7.087 | 0.00                    |
| 5             | 0.000            | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 0.00                    |
| 6             | 0.000            | 7.200 | 7.088 | 7.087 | 7.087 | 7.087 | 7.087 | 0.00                    |
| 7             | 0.000            | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 0.00                    |
| 8             | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 9             | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 10            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 11            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 12            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 13            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |       |       |       |       |       |       | RELATIVE DIFFERENCE (%) |
|---------------|------------------|-------|-------|-------|-------|-------|-------|-------------------------|
|               | 1                | 2     | 3     | 4     | 5     | 6     | 7     |                         |
| 1             | 7.200            | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 0.00                    |
| 2             | 0.000            | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 7.200 | 0.00                    |
| 3             | 0.000            | 7.200 | 7.088 | 7.087 | 7.087 | 7.087 | 7.087 | 0.00                    |
| 4             | 0.000            | 7.200 | 7.088 | 7.087 | 7.087 | 7.087 | 7.087 | 0.00                    |
| 5             | 0.000            | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 0.00                    |
| 6             | 0.000            | 7.200 | 7.088 | 7.087 | 7.087 | 7.087 | 7.087 | 0.00                    |
| 7             | 0.000            | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 5.900 | 0.00                    |
| 8             | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 9             | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 10            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 11            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 12            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |
| 13            | 0.000            | 5.904 | 6.007 | 6.008 | 6.008 | 6.008 | 6.008 | 0.00                    |

ITERATION TABLE

PARAMETER NAME: HYGIENE/S (0-10)

| SERIAL NUMBER | ITERATION NUMBER |        |        |        |        |        |        | RELATIVE DIFFERENCE (%) |
|---------------|------------------|--------|--------|--------|--------|--------|--------|-------------------------|
|               | 1                | 2      | 3      | 4      | 5      | 6      | 7      |                         |
| 1             | 10.000           | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 2             | 0.000            | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 3             | 0.000            | 10.000 | 9.804  | 9.797  | 9.706  | 9.796  | 9.796  | 0.00                    |
| 4             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 5             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 6             | 0.000            | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 0.00                    |
| 7             | 0.000            | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 0.00                    |
| 8             | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 9             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 10            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 11            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 12            | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 13            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |

| SERIAL NUMBER | ITERATION NUMBER |        |        |        |        |        |        | RELATIVE DIFFERENCE (%) |
|---------------|------------------|--------|--------|--------|--------|--------|--------|-------------------------|
|               | 1                | 2      | 3      | 4      | 5      | 6      | 7      |                         |
| 1             | 10.000           | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 2             | 0.000            | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 3             | 0.000            | 10.000 | 9.804  | 9.797  | 9.706  | 9.796  | 9.796  | 0.00                    |
| 4             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 5             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 6             | 0.000            | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 0.00                    |
| 7             | 0.000            | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 0.00                    |
| 8             | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 9             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 10            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 11            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 12            | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 13            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |

ITERATION TABLE

PARAMETER NAME: ODOUR/S (0-10)

| STREAM NUMBER | ITERATION NUMBER |        |        |        |        |        |        | RELATIVE DIFFERENCE (%) |
|---------------|------------------|--------|--------|--------|--------|--------|--------|-------------------------|
|               | 1                | 2      | 3      | 4      | 5      | 6      | 7      |                         |
| 1             | 10.000           | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 2             | 0.000            | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 3             | 0.000            | 10.000 | 9.804  | 9.797  | 9.796  | 9.796  | 9.796  | 0.00                    |
| 4             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 5             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 6             | 0.000            | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 0.00                    |
| 7             | 0.000            | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 0.00                    |
| 8             | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 9             | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 10            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 11            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 12            | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 13            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |        |        |        |        |        |        | RELATIVE DIFFERENCE (%) |
|---------------|------------------|--------|--------|--------|--------|--------|--------|-------------------------|
|               | 1                | 2      | 3      | 4      | 5      | 6      | 7      |                         |
| 1             | 10.000           | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 2             | 0.000            | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 3             | 0.000            | 10.000 | 9.804  | 9.797  | 9.796  | 9.796  | 9.796  | 0.00                    |
| 4             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 5             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 6             | 0.000            | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 0.00                    |
| 7             | 0.000            | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 5.000  | 0.00                    |
| 8             | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 9             | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 10            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 11            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 12            | 0.000            | 5.617  | 5.701  | 5.709  | 5.709  | 5.709  | 5.709  | 0.00                    |
| 13            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |

ITERATION TABLE

PARAMETER NAME: PPROT/S (0-10)

| STREAM NUMBER | ITERATION NUMBER |        |        |        |        |        |        | RELATIVE DIFFERENCE (%) |
|---------------|------------------|--------|--------|--------|--------|--------|--------|-------------------------|
|               | 1                | 2      | 3      | 4      | 5      | 6      | 7      |                         |
| 1             | 10.000           | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 2             | 0.000            | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 10.000 | 0.00                    |
| 3             | 0.000            | 10.000 | 9.804  | 9.797  | 9.796  | 9.796  | 9.796  | 0.00                    |
| 4             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 5             | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 6             | 0.000            | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 8.000  | 0.00                    |
| 7             | 0.000            | 7.000  | 7.000  | 7.000  | 7.000  | 7.000  | 7.000  | 0.00                    |
| 8             | 0.000            | 7.206  | 7.234  | 7.236  | 7.236  | 7.236  | 7.236  | 0.00                    |
| 9             | 0.000            | 7.206  | 7.234  | 7.236  | 7.236  | 7.236  | 7.236  | 0.00                    |
| 10            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 11            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |
| 12            | 0.000            | 7.206  | 7.234  | 7.236  | 7.236  | 7.236  | 7.236  | 0.00                    |
| 13            | 0.000            | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.000  | 0.00                    |

| STREAM NUMBER | ITERATION NUMBER |   |   |   |   |   |   | RELATIVE DIFFERENCE (%) |
|---------------|------------------|---|---|---|---|---|---|-------------------------|
|               | 1                | 2 | 3 | 4 | 5 | 6 | 7 |                         |
| 1             |                  |   |   |   |   |   |   |                         |
| 2             |                  |   |   |   |   |   |   |                         |
| 3             |                  |   |   |   |   |   |   |                         |
| 4             |                  |   |   |   |   |   |   |                         |
| 5             |                  |   |   |   |   |   |   |                         |
| 6             |                  |   |   |   |   |   |   |                         |
| 7             |                  |   |   |   |   |   |   |                         |

NVA - PREDES

DATE: 1980-03-28

TIME: 09.15.12

PAGE: 34

## 6. REFERENCES

The references used in model development are mainly:

1. Environmental Protection Agency:  
Short Course Proceedings  
Applications of Computer Programs in the  
Preliminary Design of Wastewater Treatment  
Facilities.  
Section I and II.  
EPA-600/2-78-185, USA, September 1978
2. Øren, K. and Balmer, P.:  
Systems Analysis of Sludge Handling.  
Progress Report No.1: Sludge Production  
NIVA/UFA, Oslo 1977
3. Eikum, A.S., Harry, C., Ofte, J. and Balmer, P.:  
Chemical Precipitation of Municipal Wastewater.  
PRA 24, Oslo 1979
4. Eikum, A.S. and Paulsrud, B.:  
Stabilization of Municipal Sludge.  
PRA 10, Oslo 1976
5. Paulsrud, B.:  
Sludge Stabilization by Lime.  
Report No.2.  
NIVA, Oslo 1975
6. Eikum, A.S.:  
Aerobic Stabilization of Primary and Mixed Primary/  
Chemical (Alum) Sludge.  
Ph.D. dissertation, University of Washington,  
Seattle, 1973